

# Drag of a thin wing and optimal shape to minimize it

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# Outline

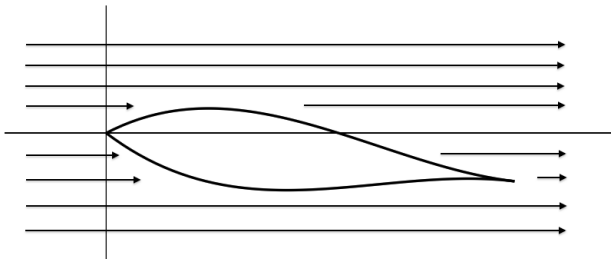
- 1 Statement of the problem
- 2 Inviscid compressible flows
- 3 Drag for supersonic case
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## Statement of the problem

A thin wing is placed at a small angle of incidence  $\alpha$  in a steady supersonic stream, so that the wing is given by:

$$y = \varepsilon f_{\pm}(x) - \alpha x, \quad \text{for } 0 < x < l$$

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Our aim is to:

- 1 Show that the drag can be approximated by

$$D = \frac{\rho_0 U^2}{B} \int_0^l \left[ (\varepsilon f'_+(x) - \alpha)^2 + (\varepsilon f'_-(x) - \alpha)^2 \right] dx$$

- 2 Confirm that the drag on a flat plate of length  $l$  at small angle of incidence  $\alpha$  is  $(2\rho_0 U^2/B)\alpha^2 l$ .
- 3 Obtain the optimal shape for a kite-form cross-section wing with given length and thickness.

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H. OCKENDON, J. R. OCKENDON, *Waves and Compressible Flow*, Text in Applied Mathematics, vol. 47, Springer, 2004

## Equations of the model

We will consider that the wing is placed in an inviscid compressible flow of a perfect gas. Therefore, we will start from the following equations:

- Continuity equation:

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{u}) = 0 \quad (\text{Cont.})$$

- Euler's equation:

$$\frac{\partial \mathbf{u}}{\partial t} + (\mathbf{u} \cdot \nabla) \mathbf{u} = -\frac{1}{\rho} \nabla p \quad (\text{Euler})$$

- Energy equation:

$$\rho \frac{de}{dt} = \frac{p}{\rho} \frac{d\rho}{dt} + \nabla \cdot (k \nabla T) + \rho \frac{dQ}{dt} \quad (\text{Energy})$$

- Perfect gas law:

$$p = \rho RT \quad (\text{Gas})$$

Besides the necessary initial state, we could also have some boundary condition (e.g., thing wing):

$$f(\mathbf{x}, t) = 0 \implies \frac{df}{dt} = \frac{\partial f}{\partial t} + \mathbf{u} \cdot \nabla f = 0$$

## Acoustics

Let us take pressure, density and temperature as perturbations:

$$p = p_0 + \bar{p} \quad \rho = \rho_0 + \bar{\rho} \quad T = T_0 + \bar{T}$$

Assuming that the barred quantities are small and neglecting *squares*:

$$(\text{Cont.}) \Rightarrow \frac{\partial \bar{p}}{\partial t} + \rho_0 \nabla \cdot \mathbf{u} + \nabla \cdot (\bar{\rho} \mathbf{u}) = 0$$

$$(\text{Euler}) \Rightarrow (\rho_0 + \bar{\rho}) \frac{\partial \mathbf{u}}{\partial t} + (\rho_0 + \bar{\rho})(\mathbf{u} \cdot \nabla) \mathbf{u} + \nabla \bar{p} = 0$$

Suppose gas is in a state of uniform motion along the  $x$  axis with some small disturbance, i.e.  $\mathbf{u} = U\mathbf{i} + \bar{\mathbf{u}}$ . Then:

$$\left( \frac{\partial}{\partial t} + U \frac{\partial}{\partial x} \right) \bar{p} + \rho_0 \nabla \cdot \bar{\mathbf{u}} = 0 \qquad \left( \frac{\partial}{\partial t} + U \frac{\partial}{\partial x} \right) \bar{\mathbf{u}} + \frac{1}{\rho_0} \nabla \bar{p} = 0$$

Note that  $c_p - c_v = R$  and denote  $\gamma = \frac{c_p}{c_v}$ . Assuming also that  $k \approx 0$  (no heat conduction):

$$(\text{Energy}) + (\text{Gas}) \Rightarrow \frac{p}{\rho^\gamma} = \frac{p_0}{\rho_0^\gamma} \Rightarrow \bar{p} = \underbrace{\frac{\gamma p_0}{\rho_0}}_{c_0^2} \bar{\rho}$$

# Acoustics

Therefore, using the three simplified equations:

$$\nabla^2 \varphi = \frac{1}{c_0^2} \left( \frac{\partial}{\partial t} + U \frac{\partial}{\partial x} \right)^2 \varphi, \quad \text{for } \varphi = \bar{p}, \bar{\rho}, \bar{\mathbf{u}}$$

In particular, for steady flows we have:

$$\nabla^2 \varphi = \frac{U^2}{c_0^2} \frac{\partial^2 \varphi}{\partial x^2} \quad (\text{Wave})$$

We denote  $M = U/c_0$ , which is called Mach number. Depending on the value of  $M$ , we distinguish two main cases:

- If  $M > 1$ , the equation is hyperbolic and the flow is said to be *supersonic*.
- If  $M < 1$ , the equation is elliptic and the flow is said to be *subsonic*.



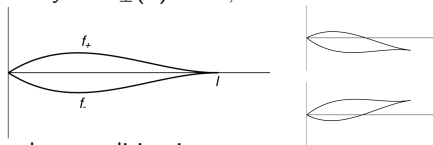
## Compressible flow past a thin wing

Now, let us consider the perturbation of  $\mathbf{u}$  of the type  $\bar{\mathbf{u}} = \varepsilon \nabla \phi$ . Then,  $\phi$  also satisfies (Wave) and from (Euler) we have:

$$p = p_0 - \varepsilon \rho_0 U \frac{\partial \phi}{\partial x}$$

Let us apply the flow to a two-dimensional thin wing, which is nearly aligned with the flow. The wing is given by:

$$y = \varepsilon f_{\pm}(x) - \alpha x, \quad \text{for } 0 < x < l$$



Therefore, the boundary condition is:

$$f'_{\pm}(x) = \frac{\partial \phi / \partial y}{U + \varepsilon \frac{\partial \phi}{\partial x}} + \frac{\alpha}{\varepsilon}, \quad \text{on } y = \varepsilon f_{\pm}(x) - \alpha x$$

And, if we suppose  $\alpha = \mathcal{O}(\varepsilon)$  (i.e.  $|\alpha| \leq C\varepsilon$ ), we have the linear approximation:

$$U f'_{\pm}(x) = \frac{\partial \phi}{\partial y} + UC, \quad \text{on } y = 0_{\pm}, \quad \text{for } 0 < x < l \quad (\text{BC})$$

## Supersonic case ( $M > 1$ )

When  $M > 1$ , the solution to

$$M^2 \frac{\partial^2 \phi}{\partial x^2} = \nabla^2 \phi$$

is of the form:

$$\phi = F(x - By) + G(x + By)$$

where  $B^2 = M^2 - 1$ . Assuming that there will be no upstream influence due to the wing, we impose:

$$\left. \frac{\partial \phi}{\partial x} \right|_{x=0} = \phi \Big|_{x=0} = 0$$

Therefore:

$$\begin{cases} \phi = \phi_+ = F(x - By), & y > 0 \\ \phi = \phi_- = G(x + By), & y < 0 \end{cases}$$

and applying boundary condition (BC) on the wing:

$$\begin{cases} -BF'(x) + UC = Uf'_+(x) \\ BG'(x) + UC = Uf'_-(x) \end{cases}, \text{ for } 0 < x < l$$

Supersonic case ( $M > 1$ )

So the solution to that is:

$$\phi_+ = -\frac{U}{B}f_+(x - By) + \frac{UC}{B}x, \quad \text{for } 0 < x - By < l, y > 0$$

$$\phi_- = \frac{U}{B}f_-(x + By) - \frac{UC}{B}x, \quad \text{for } 0 < x - By < l, y < 0$$

So now we can easily compute the drag:

$$\begin{aligned} D &= \int_0^l \left( p_+ \frac{dy_+}{dx} - p_- \frac{dy_-}{dx} \right) dx \\ &= \int_0^l \left[ \left( p_0 - \varepsilon \rho_0 U \frac{\partial \phi_+}{\partial x} \right) (\varepsilon f'_+(x) - \alpha) - \left( p_0 - \varepsilon \rho_0 U \frac{\partial \phi_-}{\partial x} \right) (\varepsilon f'_-(x) - \alpha) \right] dx \\ &= \varepsilon \rho_0 \int_0^l (f'_+(x) - f'_-(x)) dx + \varepsilon^2 \rho_0 U \int_0^l \left( -\frac{\partial \phi_+}{\partial x} f'_+(x) + \frac{\partial \phi_-}{\partial x} f'_-(x) \right) dx \\ &\quad - \alpha \varepsilon \rho_0 U \int_0^l \left( -\frac{\partial \phi_+}{\partial x} + \frac{\partial \phi_-}{\partial x} \right) dx \end{aligned}$$

## Drag of the wing

Recovering the expressions for  $\phi$ , we finally obtain:

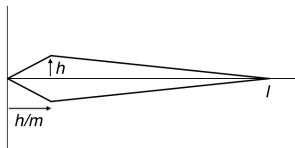
$$\begin{aligned}
 D &= \varepsilon^2 \rho_0 U \int_0^l \left[ \left( \frac{U}{B} f'_+(x) - \frac{UC}{B} \right) f'_+(x) + \left( \frac{U}{B} f'_-(x) - \frac{UC}{B} \right) f'_-(x) \right] dx \\
 &\quad - \alpha \varepsilon \rho_0 U \int_0^l \left[ \left( \frac{U}{B} f'_+(x) - \frac{UC}{B} \right) + \left( \frac{U}{B} f'_-(x) - \frac{UC}{B} \right) \right] dx \\
 &= \frac{\varepsilon^2 \rho_0 U^2}{B} \int_0^l \left[ (f'_+(x))^2 + (f'_-(x))^2 \right] dx \\
 &\quad - \frac{\varepsilon^2 \rho_0 U^2}{B} \int_0^l [C f'_+(x) + C f'_-(x)] dx \\
 &\quad - \frac{\alpha \varepsilon \rho_0 U^2}{B} \int_0^l [(f'_+(x) - C) + (f'_-(x) - C)] dx \\
 &= \frac{\rho_0 U^2}{B} \int_0^l \left[ (\varepsilon f'_+(x) - \alpha)^2 + (\varepsilon f'_-(x) - \alpha)^2 \right] dx
 \end{aligned}$$

Therefore, if we take  $\varepsilon \rightarrow 0$ , the drag on a flat plate of length  $l$  at a small angle of incidence  $\alpha$  is  $(2\rho_0 U^2/B)\alpha^2 l$ .

## Example

Suppose now that  $\alpha = 0$  and, for a given thickness  $h$ , let us consider a wing with a cross section given by:

$$f_+ = -f_- = \begin{cases} mx, & 0 < x < \frac{h}{m} \\ \frac{h(l-x)}{l-h/m}, & \frac{h}{m} < x < l \end{cases}$$



Using the formula obtained before, we have that the drag of this wing is:

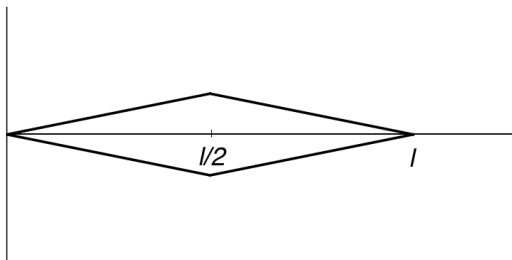
$$\begin{aligned} D &= \frac{\varepsilon^2 \rho_0 U^2}{B} \int_0^l \left[ (f'_+(x))^2 + (f'_-(x))^2 \right] dx \\ &= \frac{2\varepsilon^2 \rho_0 U^2}{B} \left[ \int_0^{\frac{h}{m}} m^2 dx + \int_{\frac{h}{m}}^l \left( \frac{h}{l-h/m} \right)^2 dx \right] \\ &= \frac{2\varepsilon^2 \rho_0 U^2}{B} \frac{m^2 hl}{ml-h} \end{aligned}$$

## Minimum drag

For  $l$  and  $h$  fixed, the minimum drag is achieved for:

$$\frac{\partial}{\partial m} \left( \frac{2\varepsilon^2 \rho_0 U^2}{B} \frac{m^2 h l}{m l - h} \right) = 0 \implies \frac{h}{m} = \frac{l}{2}$$

that corresponds to a diamond shaped wing.



Thanks for your attention!

Zorionak eta urte berri on!!

