

Shell Presentation, 11:00 am

**Simulation of Resistivity Logging Instruments  
with Mandrel Using a Self-Adaptive Goal-Oriented  
*hp*-Finite Element Method**

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L. Tabarovsky, J. Kurtz, M. Paszynski, D. Xue**

**June 14, 2005**

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**Department of Petroleum and Geosystems Engineering, and  
Institute for Computational Engineering and Sciences (ICES)  
The University of Texas at Austin**

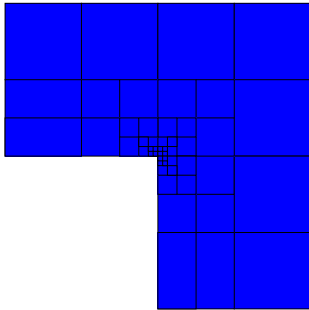
# OVERVIEW

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1. Overview
2. Main Idea of *hp* Goal-Oriented Adaptivity
3. Current Stage of the 2D High Performance FE Software
  - Flexibility
  - Reliability
  - Accuracy
  - Performance
4. Simulation of Resistivity Logging Instruments with Mandrel
5. Conclusions and Future Work (3D Problems)

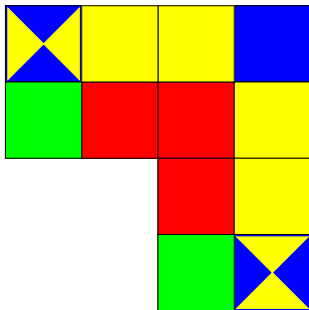
# THE $hp$ -FINITE ELEMENT METHOD

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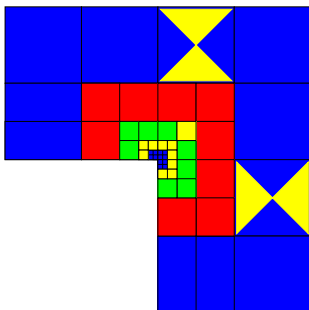
## The $h$ -Finite Element Method

1. Convergence limited by the polynomial degree, and large material contrasts.
2. Optimal  $h$ -grids do NOT converge exponentially in real applications.
3. They may “lock” (100% error).



## The $p$ -Finite Element Method

1. Exponential convergence feasible for analytical (“nice”) solutions.
2. Optimal  $p$ -grids do NOT converge exponentially in real applications.
3. If initial  $h$ -grid is not adequate, the  $p$ -method will fail miserably.

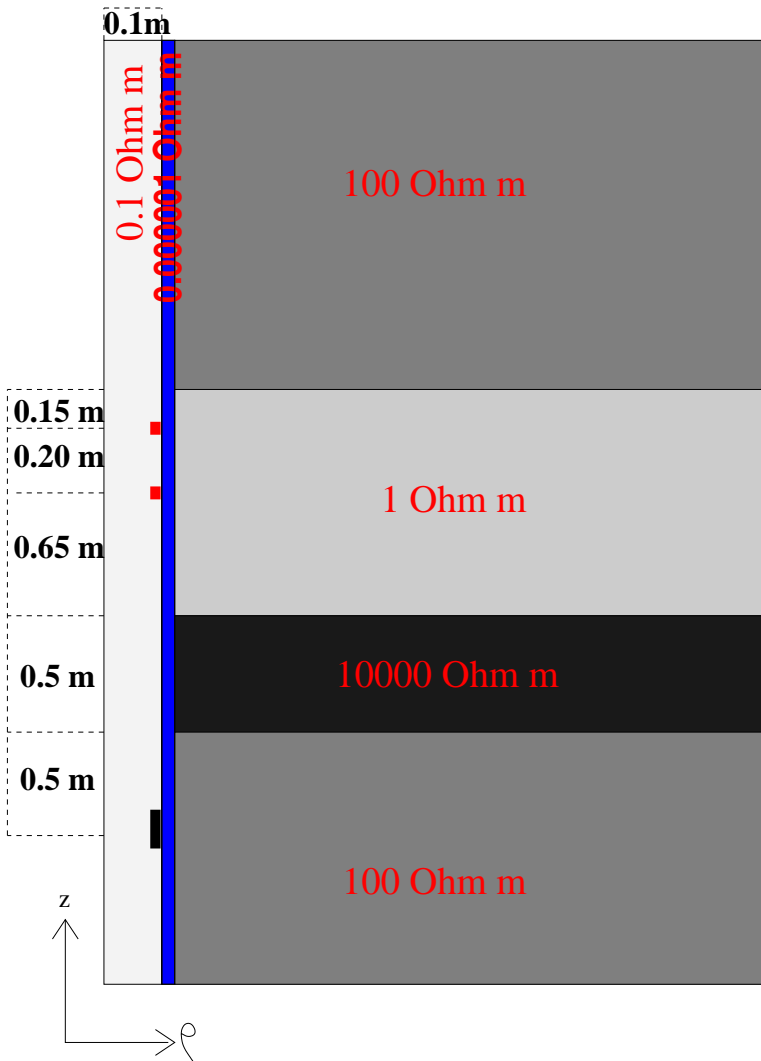


## The $hp$ -Finite Element Method

1. Exponential convergence feasible for ALL solutions.
2. Optimal  $hp$ -grids DO converge exponentially in real applications.
3. If initial  $hp$ -grid is not adequate, results will still be great.

# THE *hp*-FINITE ELEMENT METHOD

## Model Problem with Steel Casing



Frequency: 10 Hz.

Casing resistivity:  $10^{-6}$  Ohm · m.

Casing width: 0.01127 m

Discretization error < 0.1 %

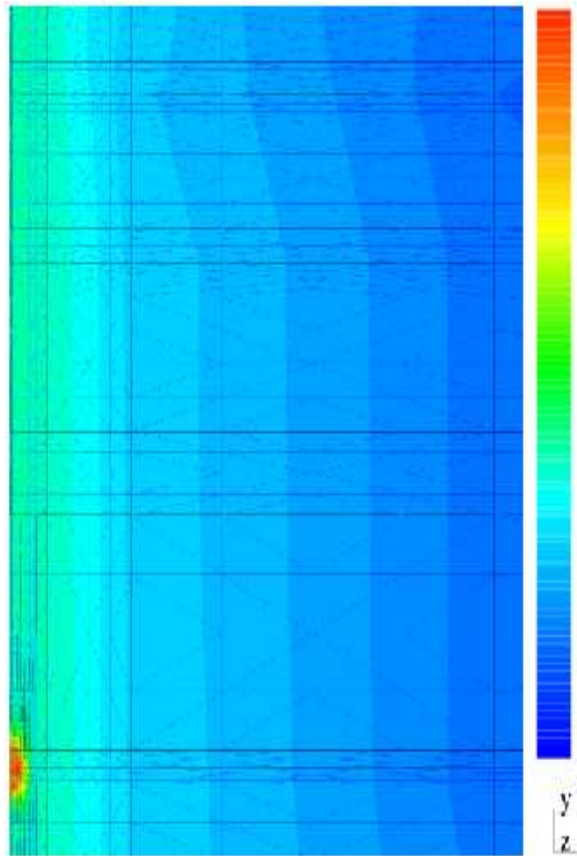
Toroidal antennas

Size (domain): 500m x 4000m

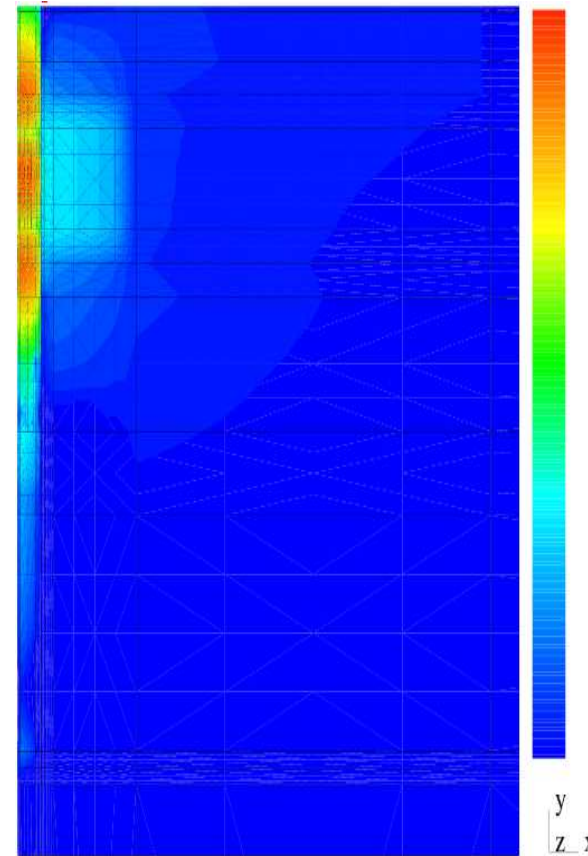
# GOAL-ORIENTED ADAPTIVITY

## Representation Formula

DIRECT PROBLEM



DUAL PROBLEM

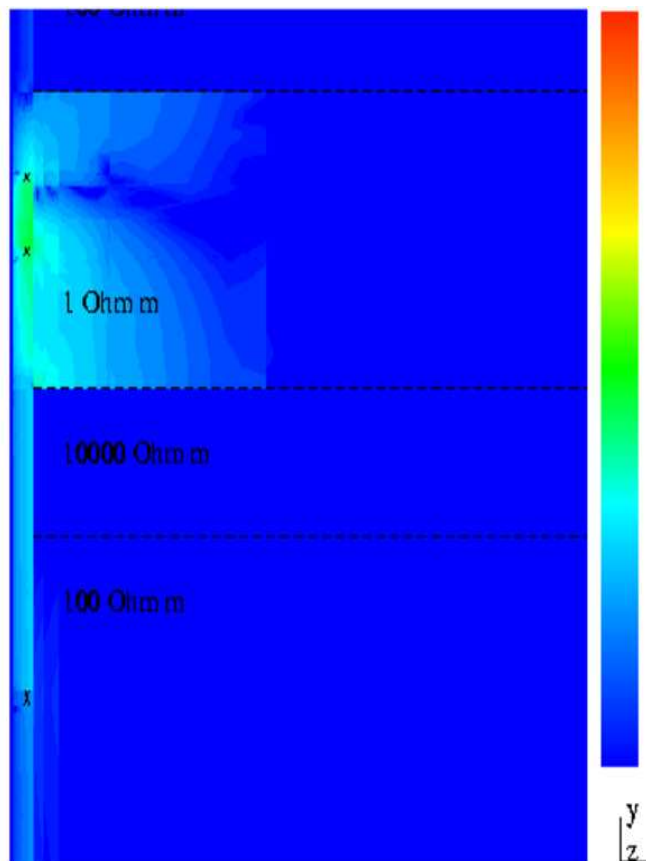


$$V = L(\Psi) = \int \bar{\sigma} \nabla \Psi \cdot \nabla G$$

# GOAL-ORIENTED ADAPTIVITY

## Movie Presentation (Sensitivity Functions)

We want to study resolution and depth of investigation of a logging instrument.



We have:  $|L(\Psi)| = \left| \int S \, dV \right| \leq \int |S| \, dV$ .

In the next movies, we display:  $\log_{10} |S|$ .

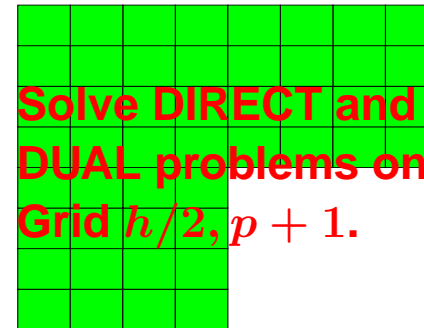
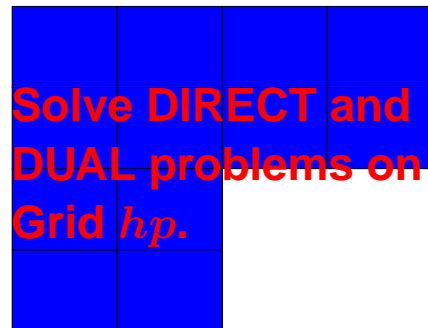
Scales:

- Red  $\rightarrow |S| = |L(\Psi)| * 10^4$ .
- Blue  $\rightarrow |S| = |L(\Psi)| * 10^{-2}$ .

Direct Current

# SELF-ADAPTIVE GOAL-ORIENTED $hp$ -FEM

## Algorithm for Goal-Oriented Adaptivity

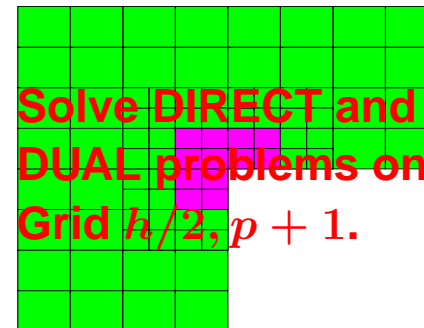
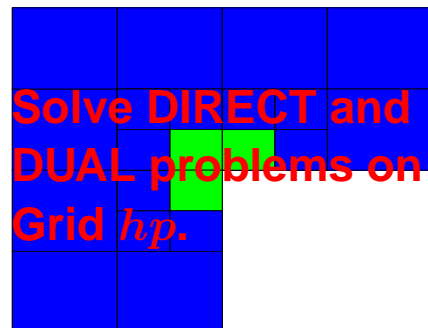


Compute  $e = \Psi_{h/2,p+1} - \Psi_{hp}$ , and  $\tilde{e} = \Psi_{h/2,p+1} - \Pi_{hp} \Psi_{h/2,p+1}$ .

Compute  $\epsilon = G_{h/2,p+1} - G_{hp}$ , and  $\tilde{\epsilon} = G_{h/2,p+1} - \Pi_{hp} G_{h/2,p+1}$ .

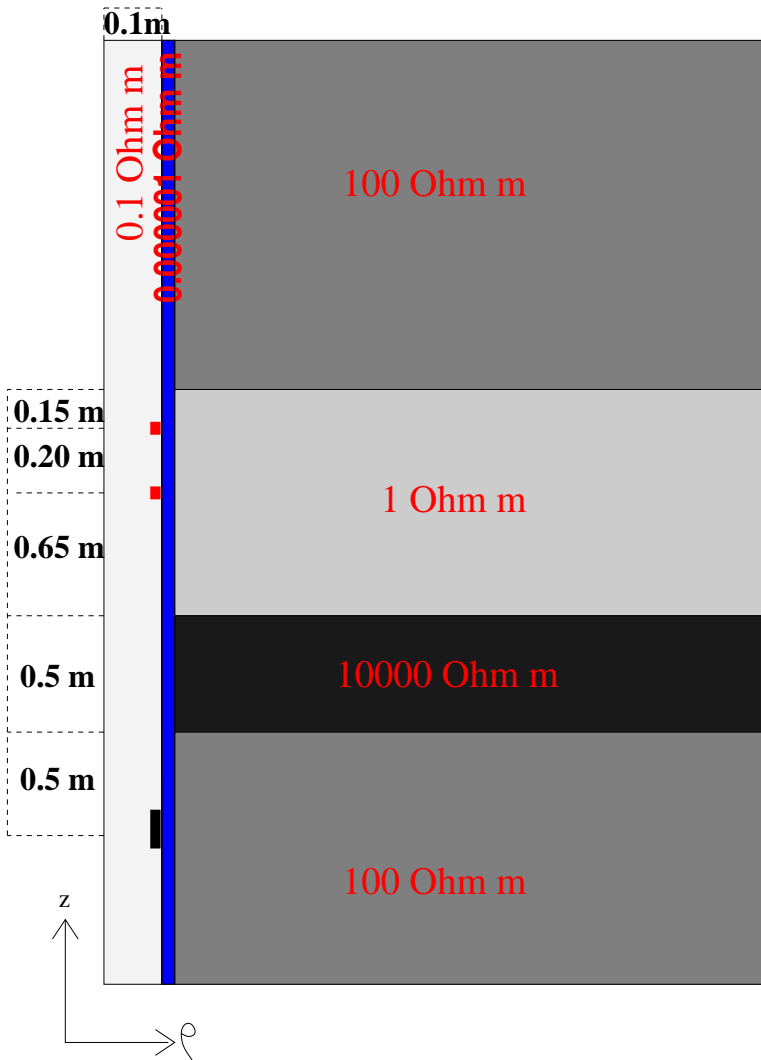
$$|L(e)| = |b(e, \epsilon)| \sim |b(\tilde{e}, \tilde{\epsilon})| \leq \sum_K |b_K(\tilde{e}, \tilde{\epsilon})| \leq \sum_K \|\tilde{e}\|_{E,K} \|\tilde{\epsilon}\|_{E,K}.$$

Apply the fully automatic  $hp$ -adaptive algorithm.



# SELF-ADAPTIVE GOAL-ORIENTED $hp$ -FEM

## Model Problem with Steel Casing



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Discretization error < 0.1 %

Toroidal antennas

Size (domain): 500m x 4000m



# CURRENT STAGE OF THE 2D *hp*-FE SOFTWARE

## Flexibility (What Problems Can We Solve?)

### Time-Harmonic Maxwell's Equations

$\nabla \times \mathbf{H} = (\bar{\sigma} + j\omega\bar{\epsilon})\mathbf{E} + \mathbf{J}^{imp}$	<b>Ampere's law</b>
$\nabla \times \mathbf{E} = -j\omega\bar{\mu}\mathbf{H} - \mathbf{M}^{imp}$	<b>Faraday's law</b>
$\nabla \cdot (\bar{\epsilon}\mathbf{E}) = \rho$	<b>Gauss' law of Electricity</b>
$\nabla \cdot (\bar{\mu}\mathbf{H}) = 0$	<b>Gauss' law of Magnetism</b>

### E-VARIATIONAL FORMULATION:

$$\left\{ \begin{array}{l} \text{Find } \mathbf{E} \in \mathbf{E}_D + \mathbf{H}_D(\text{curl}; \Omega) \text{ such that:} \\ \int_{\Omega} (\bar{\mu}^{-1} \nabla \times \mathbf{E}) \cdot (\nabla \times \bar{\mathbf{F}}) dV - \int_{\Omega} (\bar{k}^2 \mathbf{E}) \cdot \bar{\mathbf{F}} dV = -j\omega \int_{\Omega} \mathbf{J}^{imp} \cdot \bar{\mathbf{F}} dV \\ + j\omega \int_{\Gamma_N} \mathbf{J}_{\Gamma_N}^{imp} \cdot \bar{\mathbf{F}}_t dS - \int_{\Omega} (\bar{\mu}^{-1} \mathbf{M}^{imp}) \cdot (\nabla \times \bar{\mathbf{F}}) dV \quad \forall \mathbf{F} \in \mathbf{H}_D(\text{curl}; \Omega) \end{array} \right.$$

# CURRENT STAGE OF THE 2D $hp$ -FE SOFTWARE

## Flexibility (What Problems Can We Solve?)

### AXISYMMETRIC PROBLEMS

#### $E_\phi$ -Variational Formulation (Azimuthal)

$$\left\{ \begin{array}{l} \text{Find } E_\phi \in E_{\phi,D} + \tilde{H}_D^1(\Omega) \text{ such that:} \\ \int_{\Omega} (\bar{\mu}_{\rho,z}^{-1} \nabla \times E_\phi) \cdot (\nabla \times \bar{F}_\phi) dV - \int_{\Omega} (\bar{k}_\phi^2 E_\phi) \cdot \bar{F}_\phi dV = -j\omega \int_{\Omega} J_\phi^{imp} \bar{F}_\phi dV \\ + j\omega \int_{\Gamma_N} J_{\phi,\Gamma_N}^{imp} \bar{F}_\phi dS - \int_{\Omega} (\bar{\mu}_{\rho,z}^{-1} M_{\rho,z}^{imp}) \cdot \bar{F}_\phi dV \quad \forall F_\phi \in \tilde{H}_D^1(\Omega) \end{array} \right.$$

#### $E_{\rho,z}$ -Variational Formulation (Meridian)

$$\left\{ \begin{array}{l} \text{Find } (E_\rho, E_z) \in E_D + \tilde{H}_D(\text{curl}; \Omega) \text{ such that:} \\ \int_{\Omega} (\bar{\mu}_\phi^{-1} \nabla \times E_{\rho,z}) \cdot (\nabla \times \bar{F}_{\rho,z}) dV - \int_{\Omega} (\bar{k}_{\rho,z}^2 E_{\rho,z}) \cdot \bar{F}_{\rho,z} dV = \\ -j\omega \int_{\Omega} J_\rho^{imp} \bar{F}_\rho + J_z^{imp} \bar{F}_z dV + j\omega \int_{\Gamma_N} J_{\rho,\Gamma_N}^{imp} \bar{F}_\rho + J_{z,\Gamma_N}^{imp} \bar{F}_z dS \\ - \int_{\Omega} (\bar{\mu}_\phi^{-1} M_\phi^{imp}) \cdot \bar{F}_{\rho,z} dV \quad \forall (F_\rho, F_z) \in \tilde{H}_D(\text{curl}; \Omega) \end{array} \right.$$

## **CURRENT STAGE OF THE 2D *hp*-FE SOFTWARE**

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### **Flexibility (What Problems Can We Solve?)**

- **Physical Devices: Casing, Casing Imperfections, Mandrel, Magnetic Buffers, Insulators, Displacement Currents, Combination of All, etc.**
- **Materials: Isotropic, Anisotropic\*.**
- **Sources: Toroidal Antennas, Solenoidal Antennas, Dipoles in Any Direction, Electrodes, Finite Size Antennas, Combination of All, etc.**
- **Logging Instruments: Logging While Drilling (LWD), Laterolog, Normal, Induction, Dielectric Instruments, Cross-well, etc.**
- **Any Frequency (0-10 Ghz).**

**ALL AXISYMMETRIC RESISTIVITY LOGGING PROBLEMS**

# CURRENT STAGE OF THE 2D $hp$ -FE SOFTWARE

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## Reliability (Can We Trust the Solutions?)

- **Comparison Against Analytical Results.**
  1. Exact solution in a homogeneous media.
  2. Exact solution in a homogeneous media with a mandrel.
  3. Exact solution in a homogeneous media with casing.
- **Verification of Physical Properties.**
  1. Reciprocity principle (Gregory Itskovich).
  2. Discrete divergence free approximation for edge elements.
- **Numerical Verifications.**
  1. Different size of domain and antennas.
  2. Comparison against other numerical software (Yang Wei).
  3. Error control provided by the fine grid solution.
  4. Comparison between continuous elements vs. edge elements.

## CURRENT STAGE OF THE 2D $hp$ -FE SOFTWARE

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### Reliability (Can We Trust the Solutions?)

Problem with casing at 10 kHz.

#### Continuous Elements

Quantity of Interest	Real Part	Imag Part
COARSE GRID	0.1516098429E-08	-0.1456374493E-08
FINE GRID	0.1516094029E-08	-0.1456390824E-08

#### Edge Elements

Quantity of Interest	Real Part	Imag Part
COARSE GRID	0.1516060872E-08	-0.1456337248E-08
FINE GRID	0.1516093804E-08	-0.1456390864E-08

**Error control provided by the fine grid solution.**

## CURRENT STAGE OF THE 2D $hp$ -FE SOFTWARE

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**Comparison between continuous elements vs. edge elements.**

# CURRENT STAGE OF THE 2D $hp$ -FE SOFTWARE

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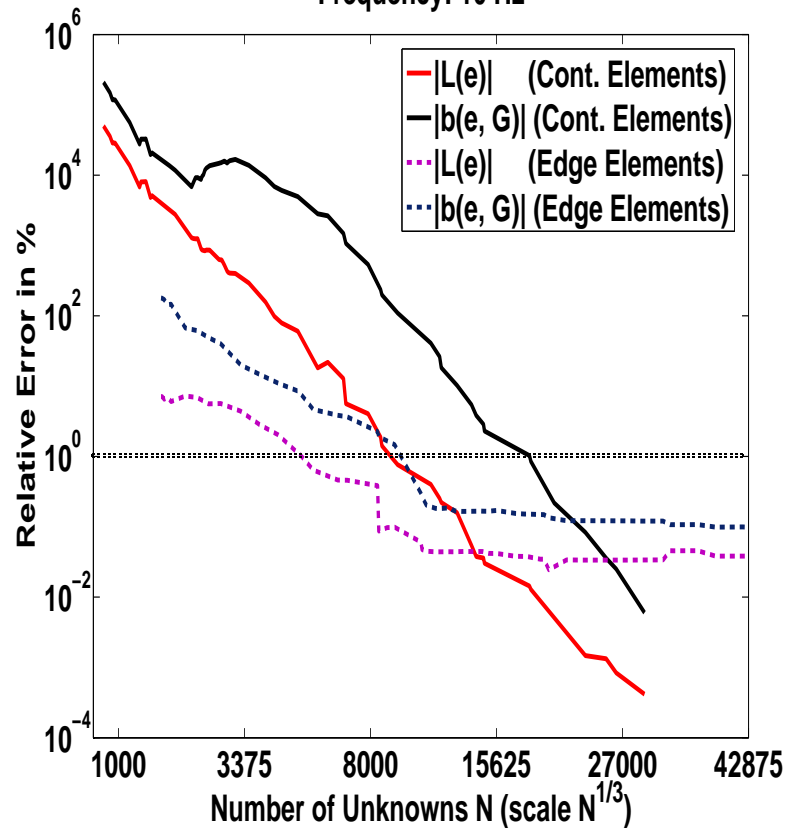
**HIGHLY RELIABLE SOFTWARE**

# CURRENT STAGE OF THE 2D $hp$ -FE SOFTWARE

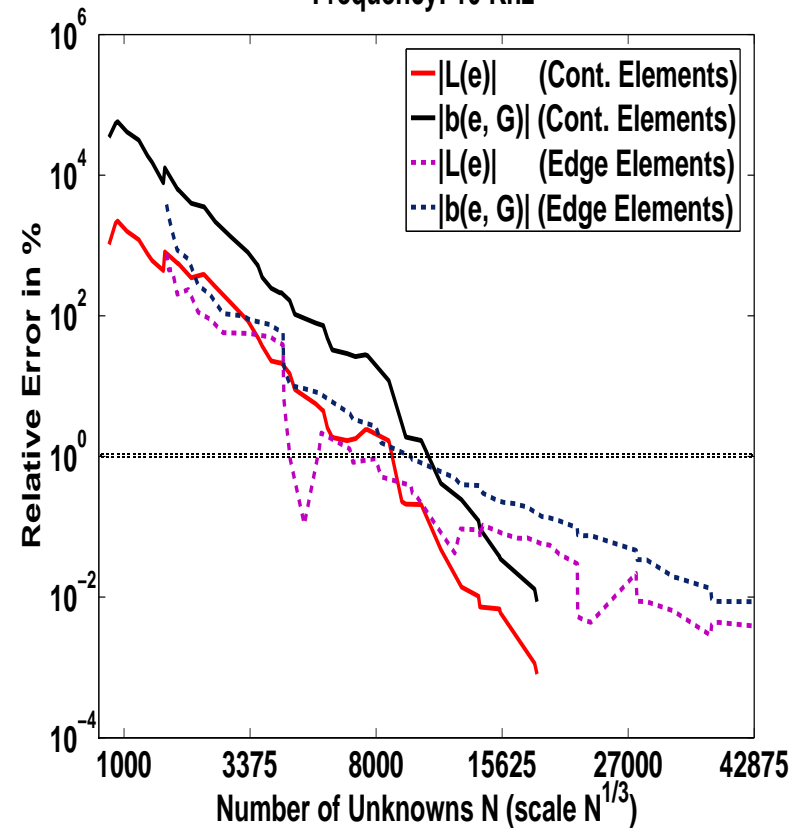
## Accuracy (Are the Solutions Accurate?)

### Problem with Casing (Convergence Curve)

Frequency: 10 Hz



Frequency: 10 KHz



**EXTREMELY ACCURATE SOFTWARE**



## CURRENT STAGE OF THE 2D *hp*-FE SOFTWARE

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### Performance (How Fast Can We Solve the Problems?)

80 Vert. Pos.	$10^{-6}\Omega \cdot m$	$10^{-5}\Omega \cdot m$
Toroid (10 KHz)	19' 46"	16' 28"
Ring of Vert. Dipoles (10 KHz)	22' 47"	17' 02"
Ring of Horiz. Dipoles (10 KHz)	19' 25"	13' 25"
Electrodes (0 Hz)	10' 10"	8' 35"

IBM Power 4 compiler 1.3 Ghz (4 years old)

Possible improvements in performance:

- To use a 3.4 Ghz processor.
- To execute the code in 8 processors (10 positions per processor).
- To improve implementation.

**HIGH PERFORMANCE SOFTWARE**

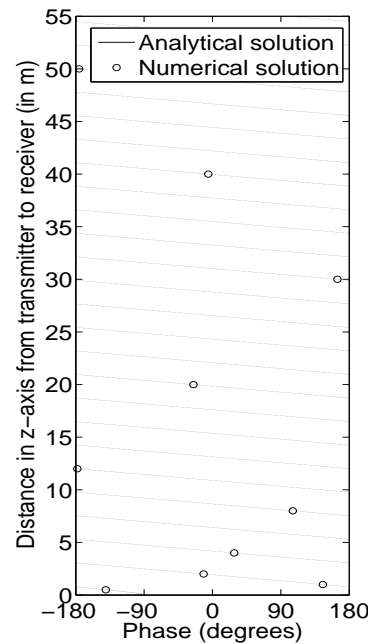
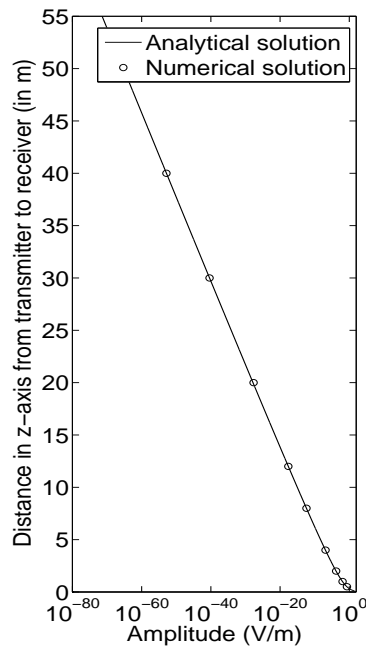
# SIMULATION OF LOGGING INSTRUMENTS

## Comparison Against Analytical Solutions

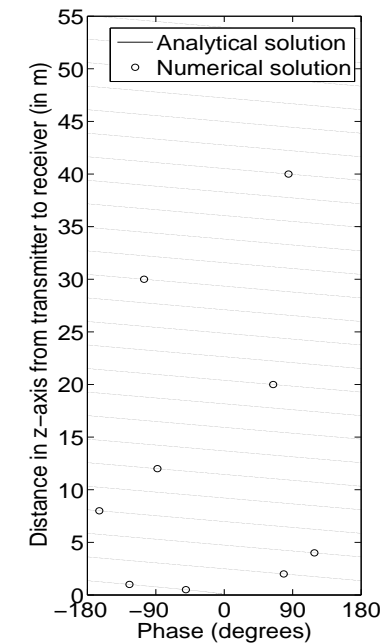
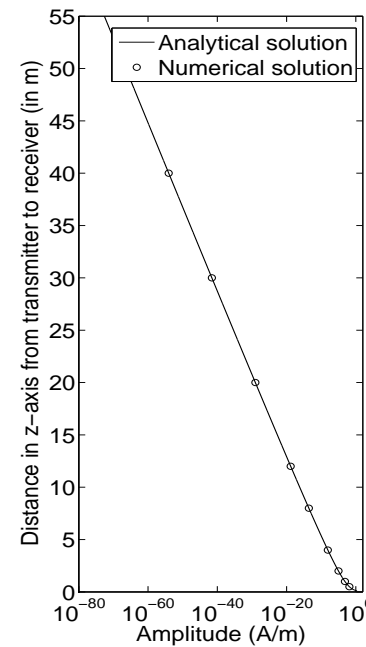
Solutions in a Homogeneous Lossy ( $1 \Omega m$ ) Media (2 Mhz)

Solenoid Antenna

Toroid Antenna



Electric Field



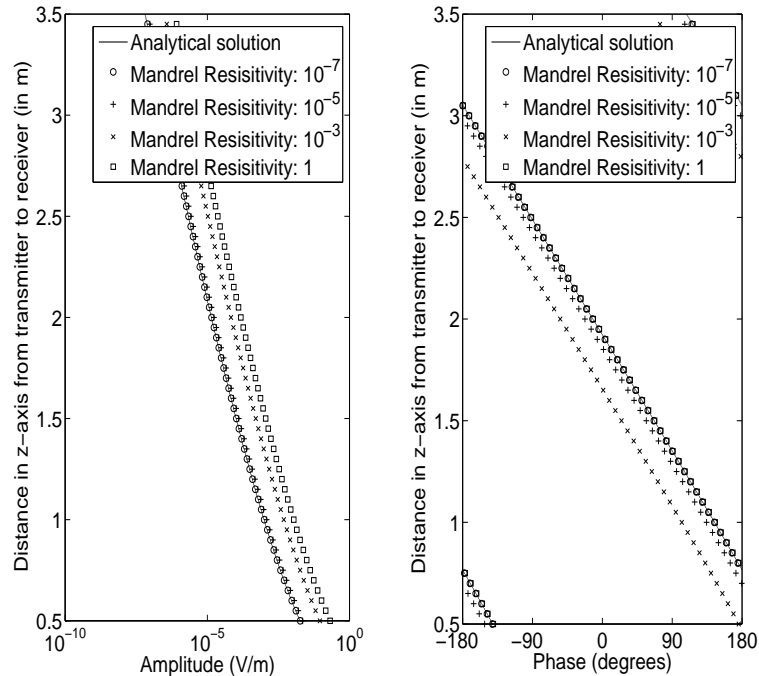
Magnetic Field

# SIMULATION OF LOGGING INSTRUMENTS

## Comparison Against Analytical Solutions

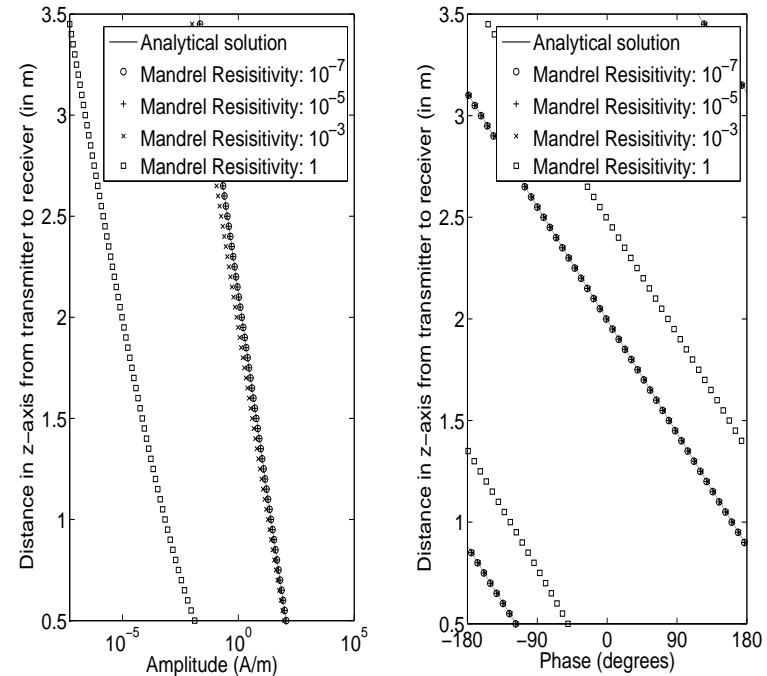
Solutions in a Homogeneous Lossy ( $1 \Omega m$ ) Media (2 Mhz) in Presence of a Conductive Mandrel

### Solenoid Antenna



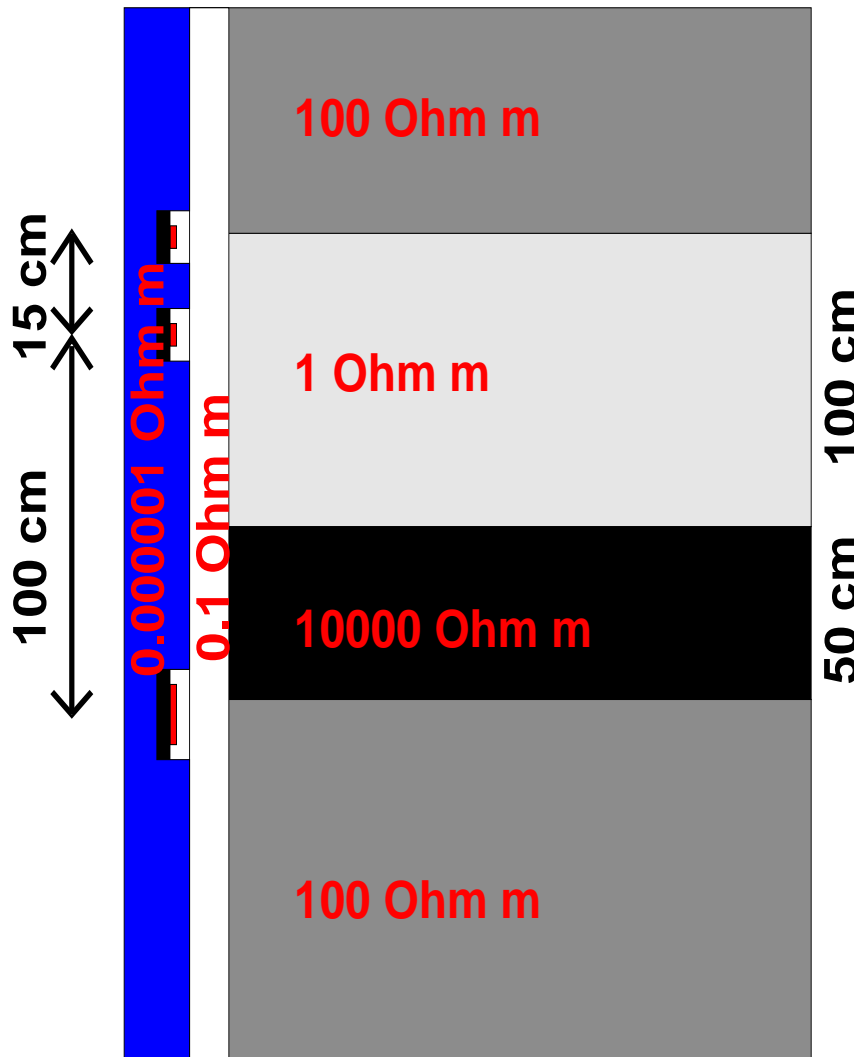
### Electric Field

### Toroid Antenna

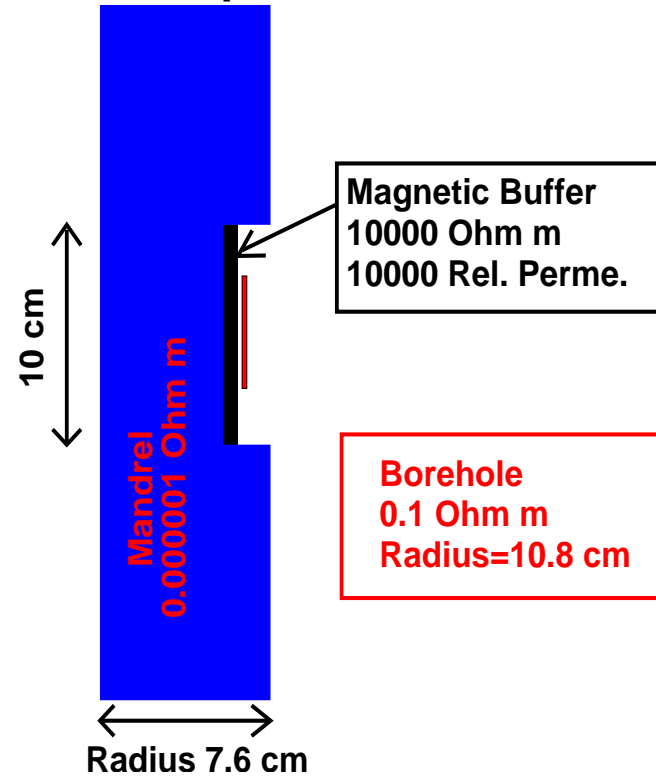


### Magnetic Field

# SIMULATION OF LOGGING INSTRUMENTS



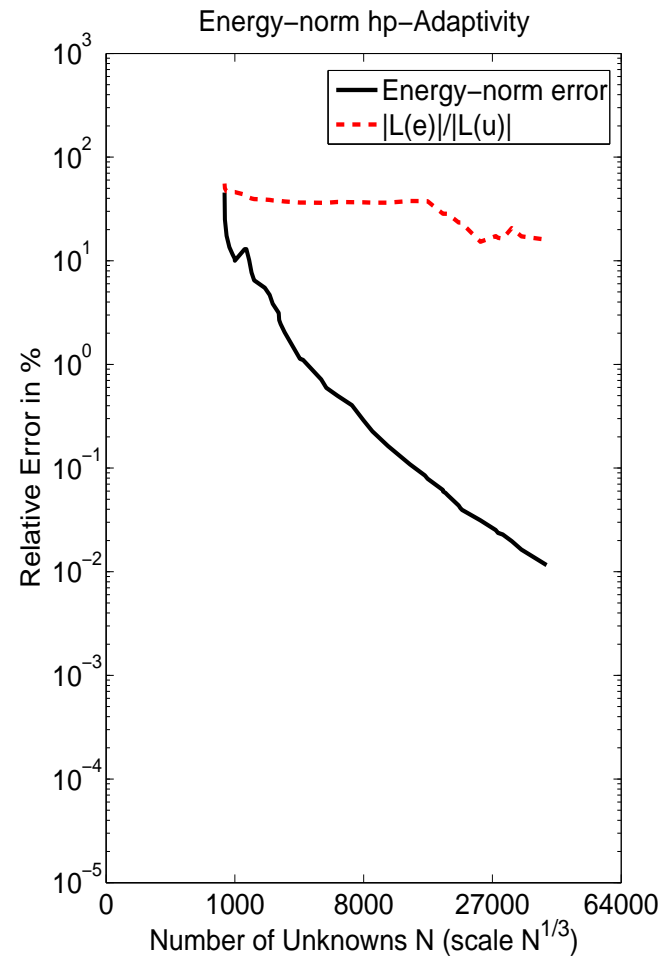
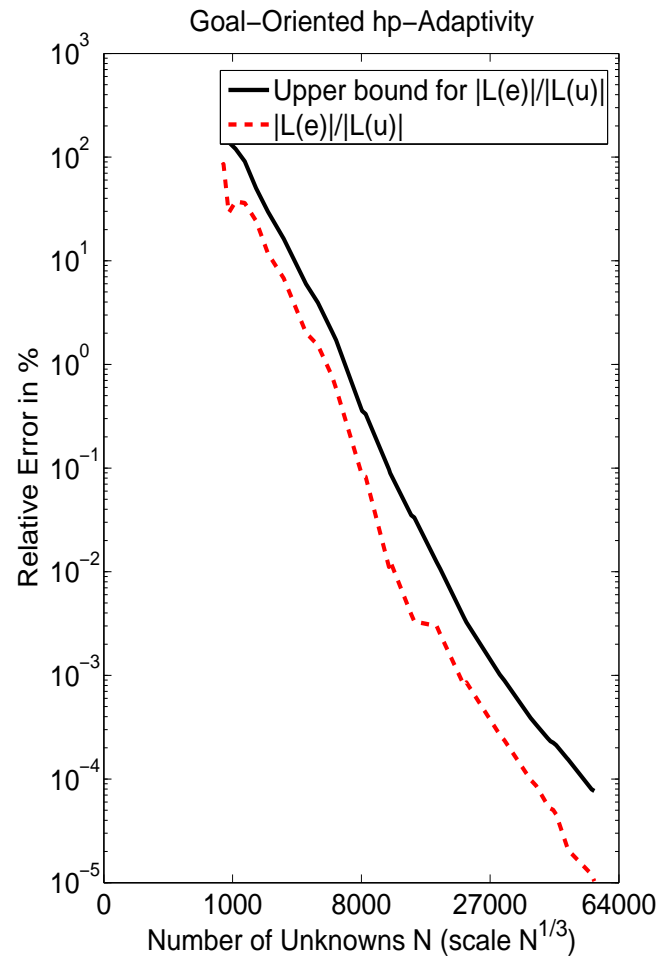
## Description of Antennas



**Goal: To Compute First  
Difference of Potential  
on Receiving Antennas**

# SIMULATION OF LOGGING INSTRUMENTS

## First. Vert. Diff. $E_\phi$ (solenoid). Position: 0.475m



# SIMULATION OF LOGGING INSTRUMENTS

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## Goal-Oriented vs. Energy-norm *hp*-Adaptivity

Problem with Mandrel at 2 Mhz.

### Continuous Elements (Goal-Oriented Adaptivity)

Quantity of Interest	Real Part	Imag Part
COARSE GRID	-0.1629862203E-01	-0.4016944732E-02
FINE GRID	-0.1629862347E-01	-0.4016944223E-02

### Continuous Elements (Energy-norm Adaptivity)

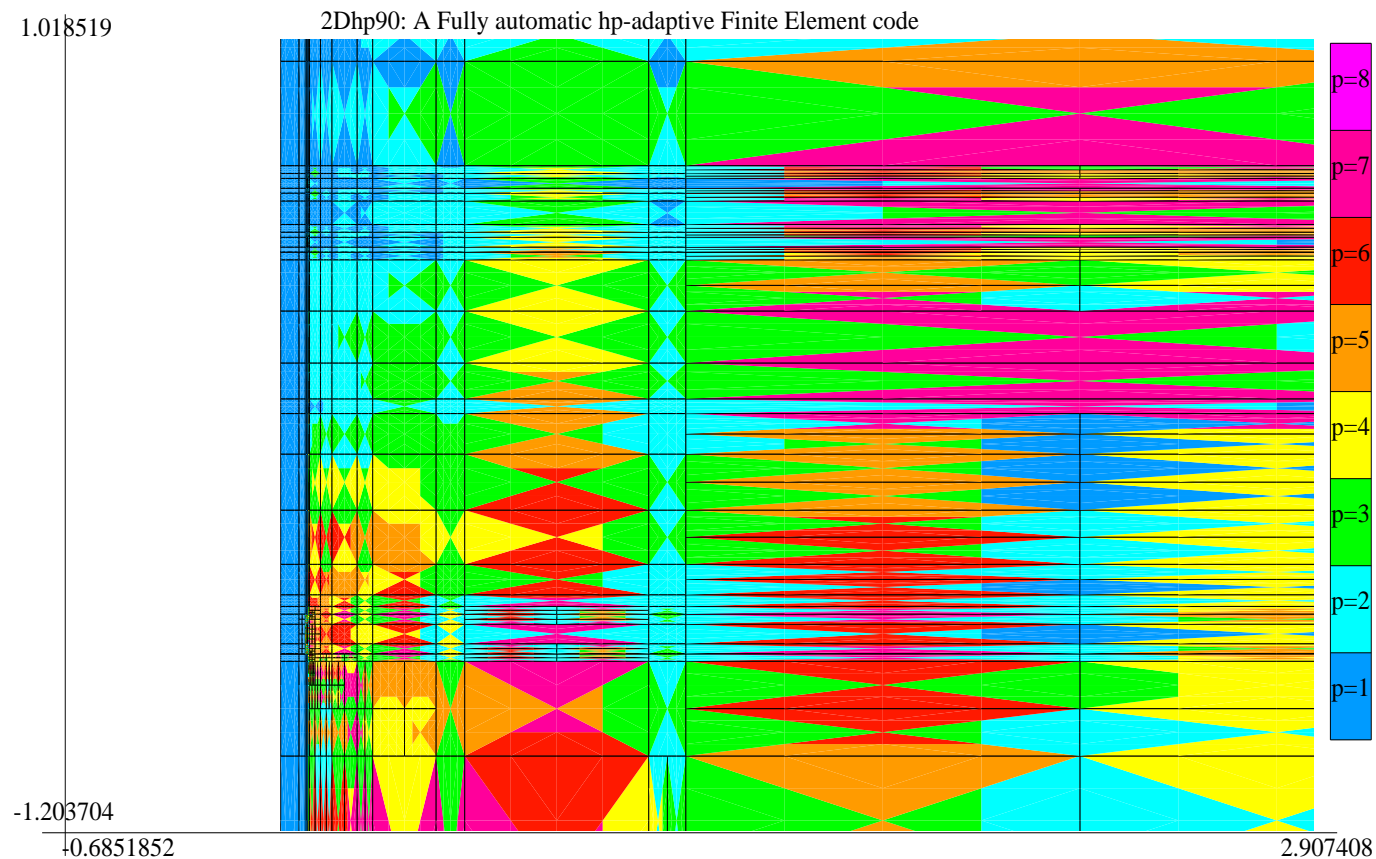
Quantity of Interest	Real Part	Imag Part
0.01% ENERGY ERROR	-0.1382759158E-01	-0.2989492851E-02

**It is critical to use GOAL-ORIENTED adaptivity.**

# SIMULATION OF LOGGING INSTRUMENTS

First. Vert. Diff.  $E_\phi$  (solenoid). Position: 0.475m

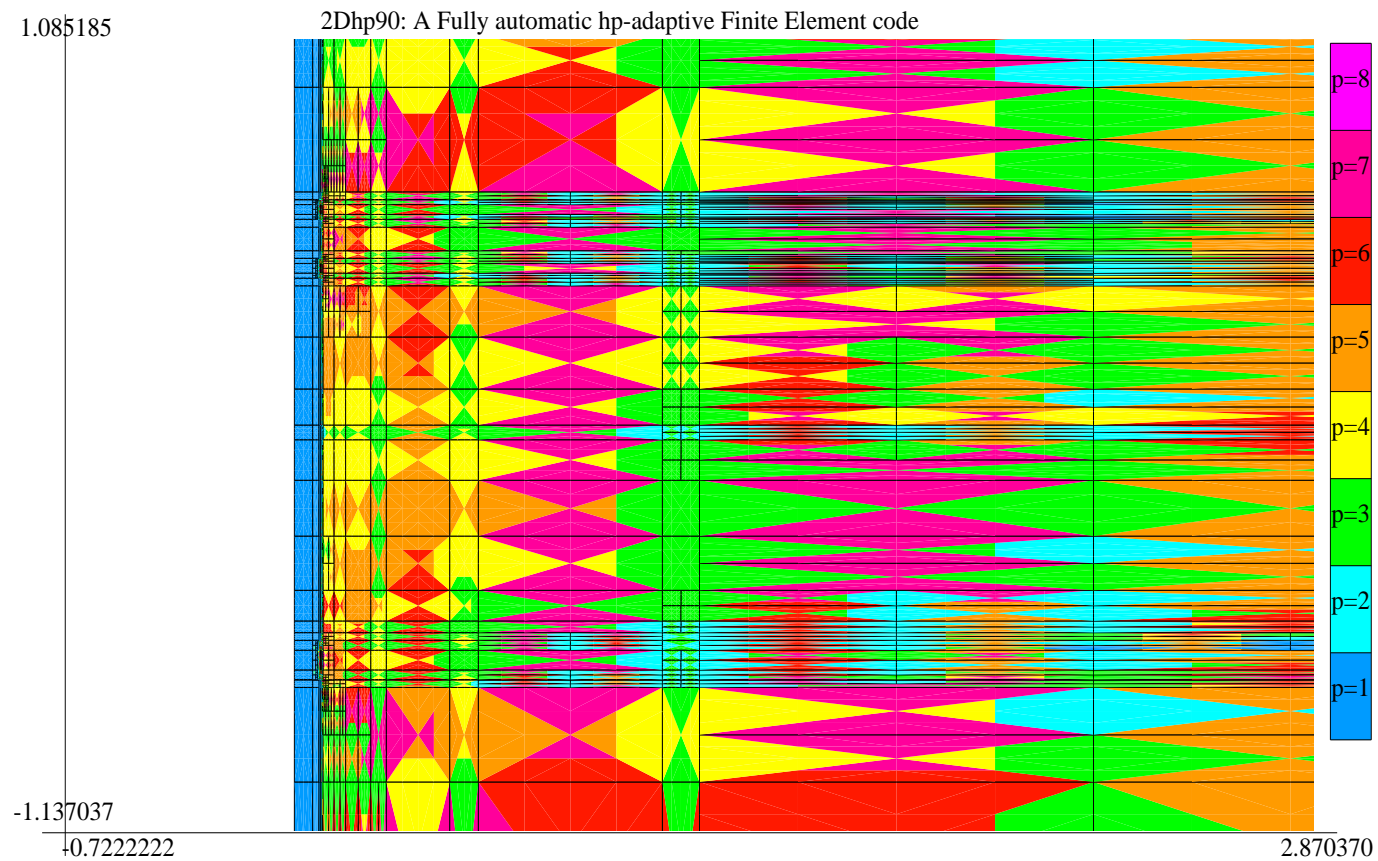
ENERGY-NORM HP-ADAPTIVITY



# SIMULATION OF LOGGING INSTRUMENTS

First. Vert. Diff.  $E_\phi$  (solenoid). Position: 0.475m

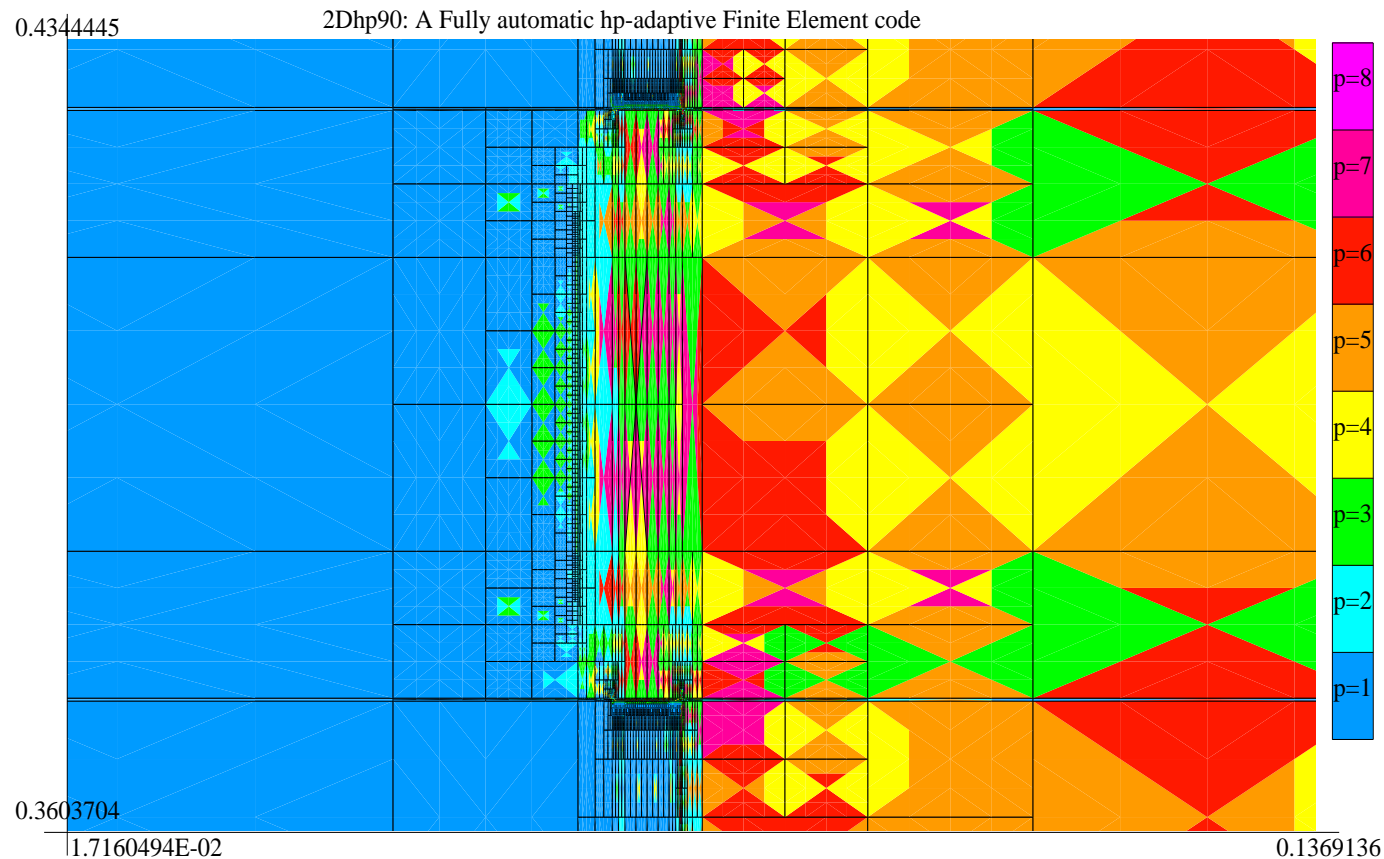
GOAL-ORIENTED HP-ADAPTIVITY





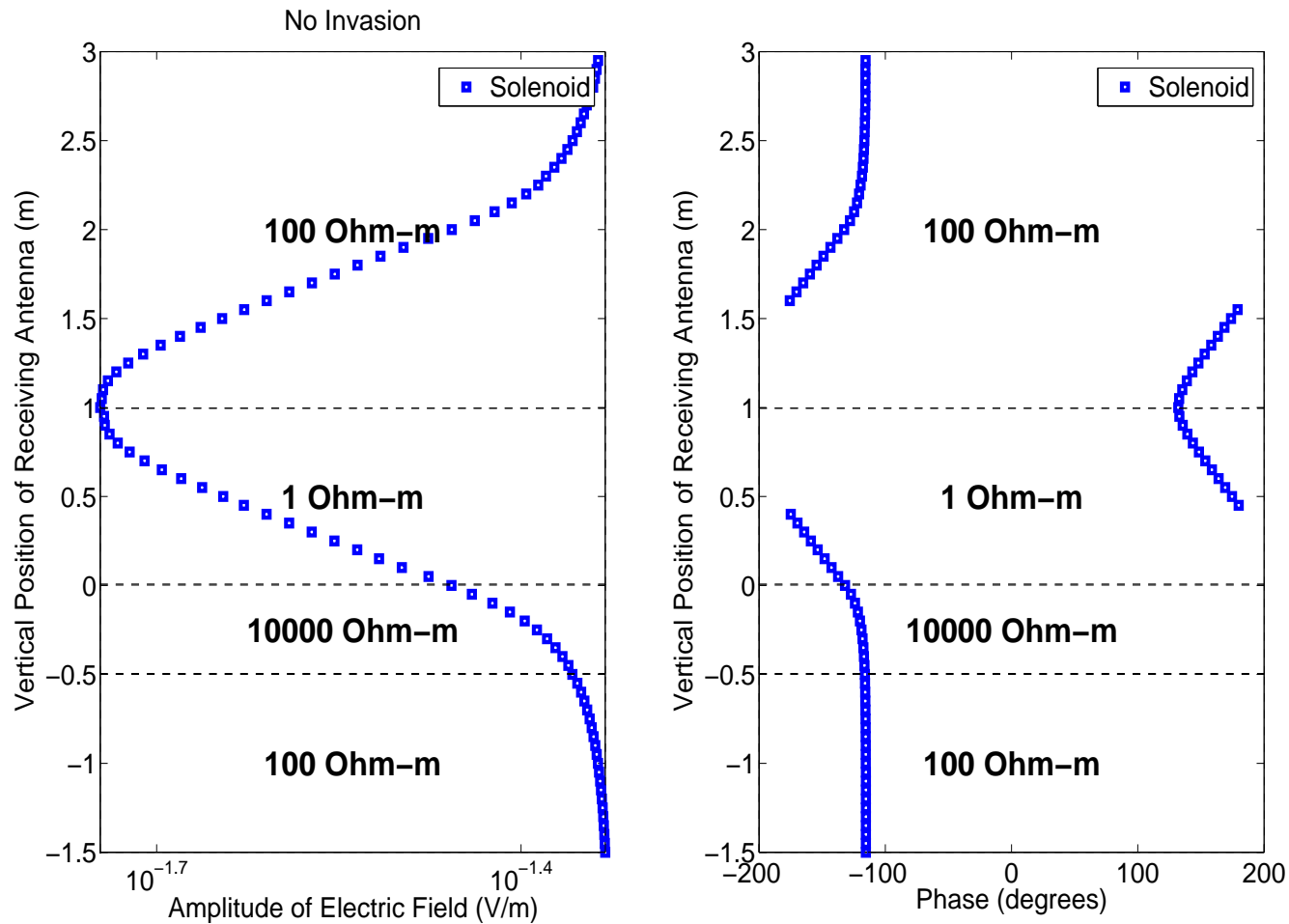
# SIMULATION OF LOGGING INSTRUMENTS

First. Vert. Diff.  $E_\phi$  (solenoid). Position: 0.475m  
GOAL-ORIENTED HP-ADAPTIVITY (ZOOM TOWARDS FIRST RECEIVER ANTENNA)



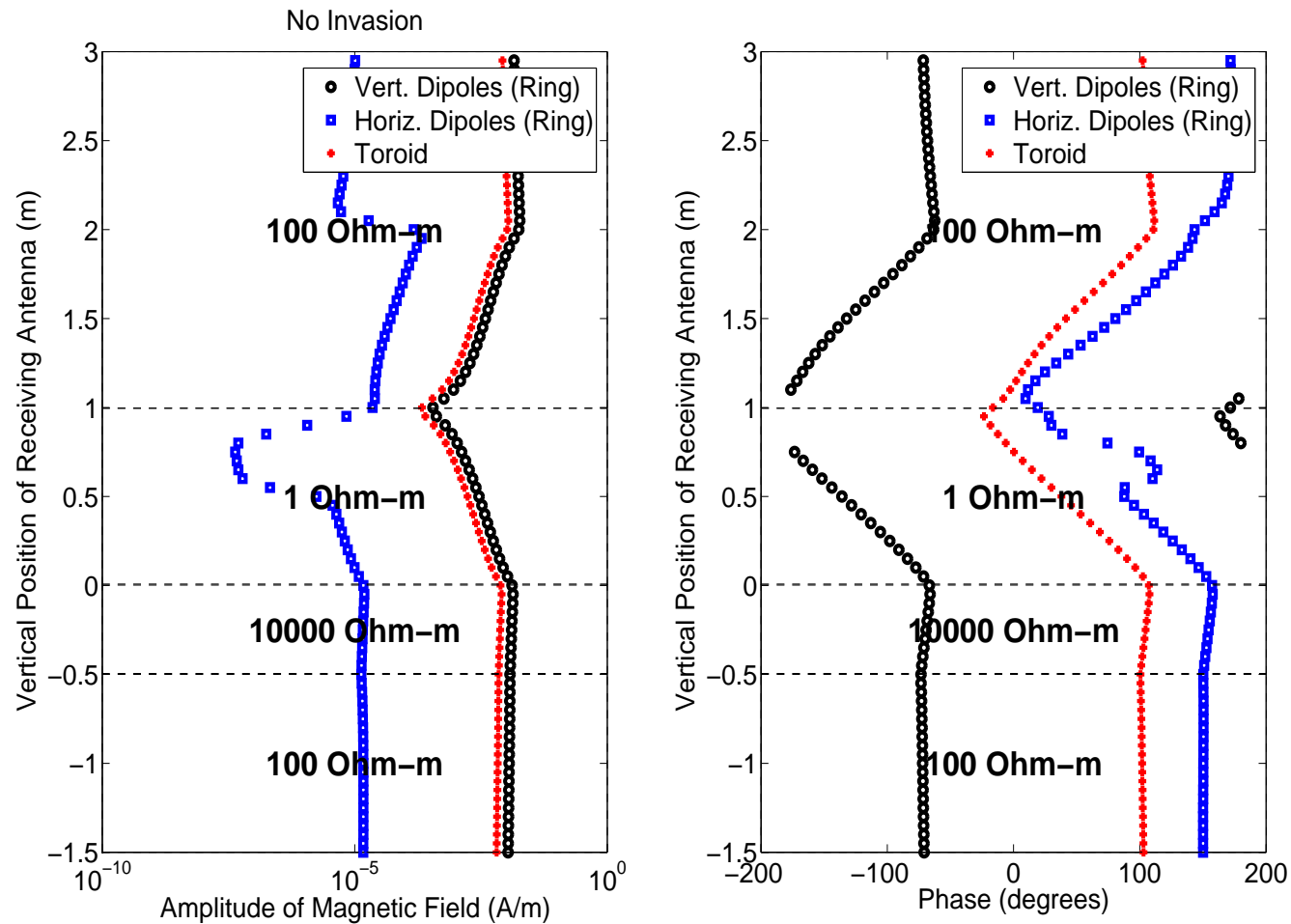
# SIMULATION OF LOGGING INSTRUMENTS

## $E_\phi$ for a solenoid antenna



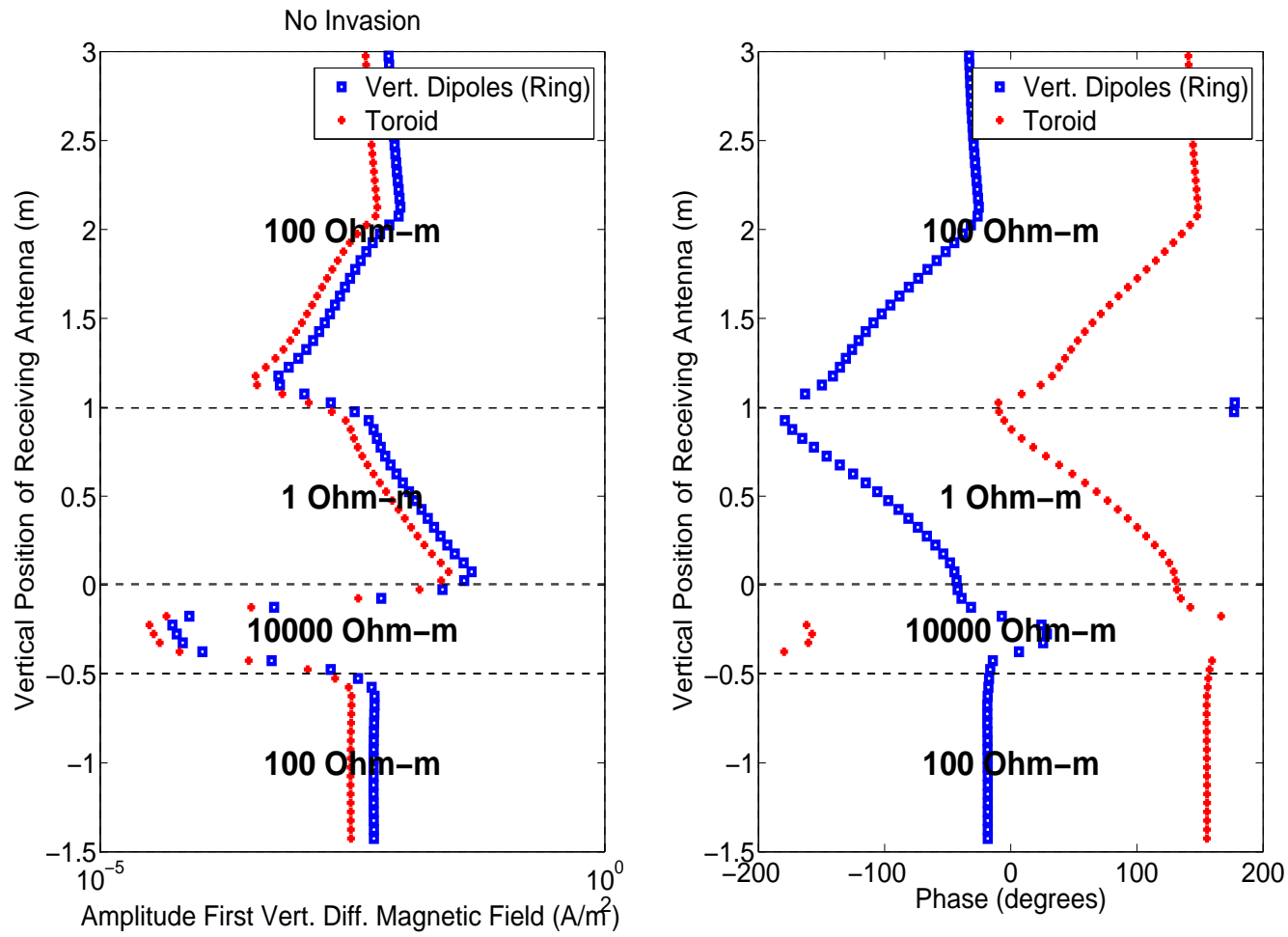
# SIMULATION OF LOGGING INSTRUMENTS

## $H_\phi$ for different antennas



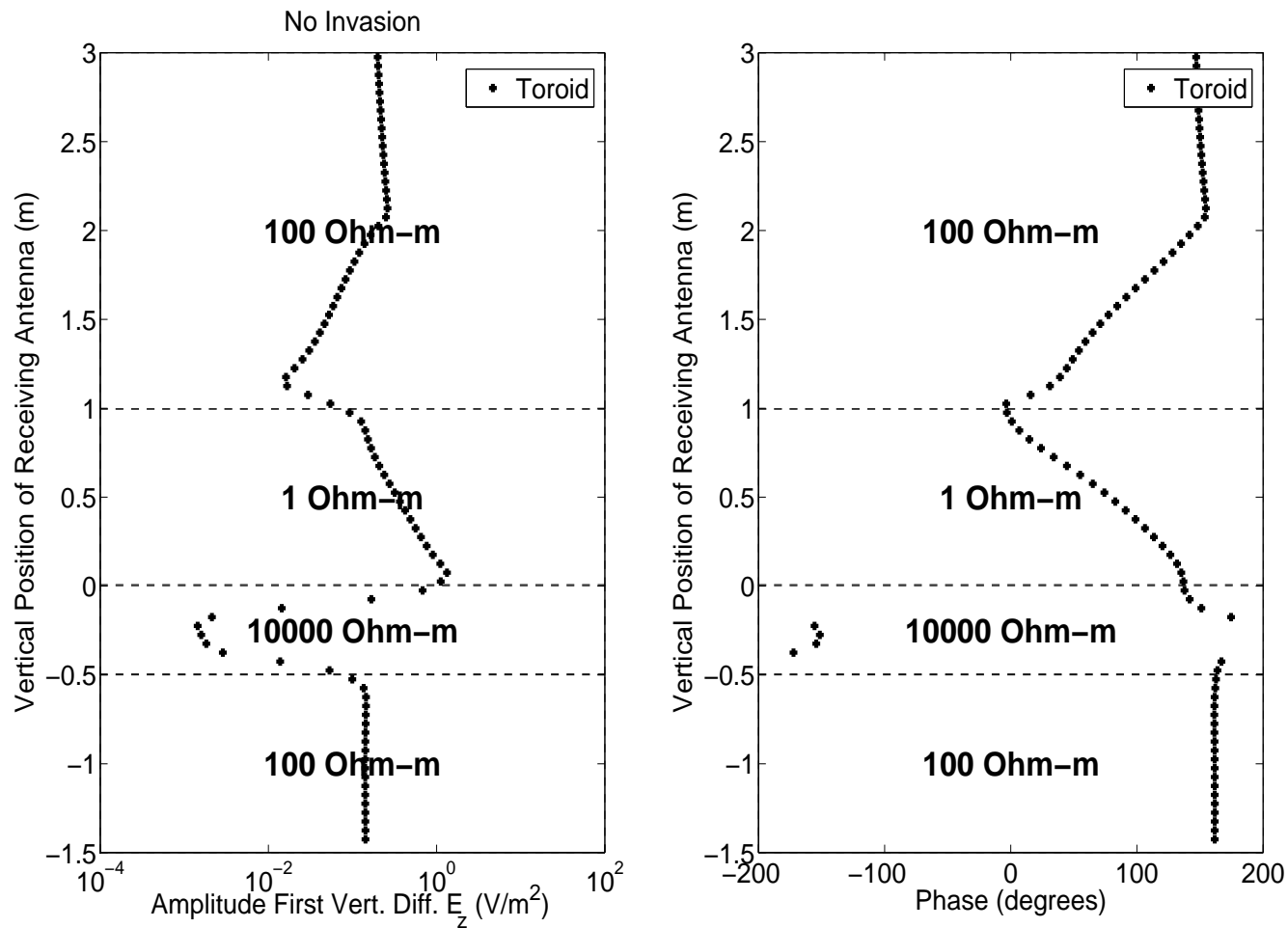
# SIMULATION OF LOGGING INSTRUMENTS

## First Vert. Diff. $H_\phi$ for different antennas



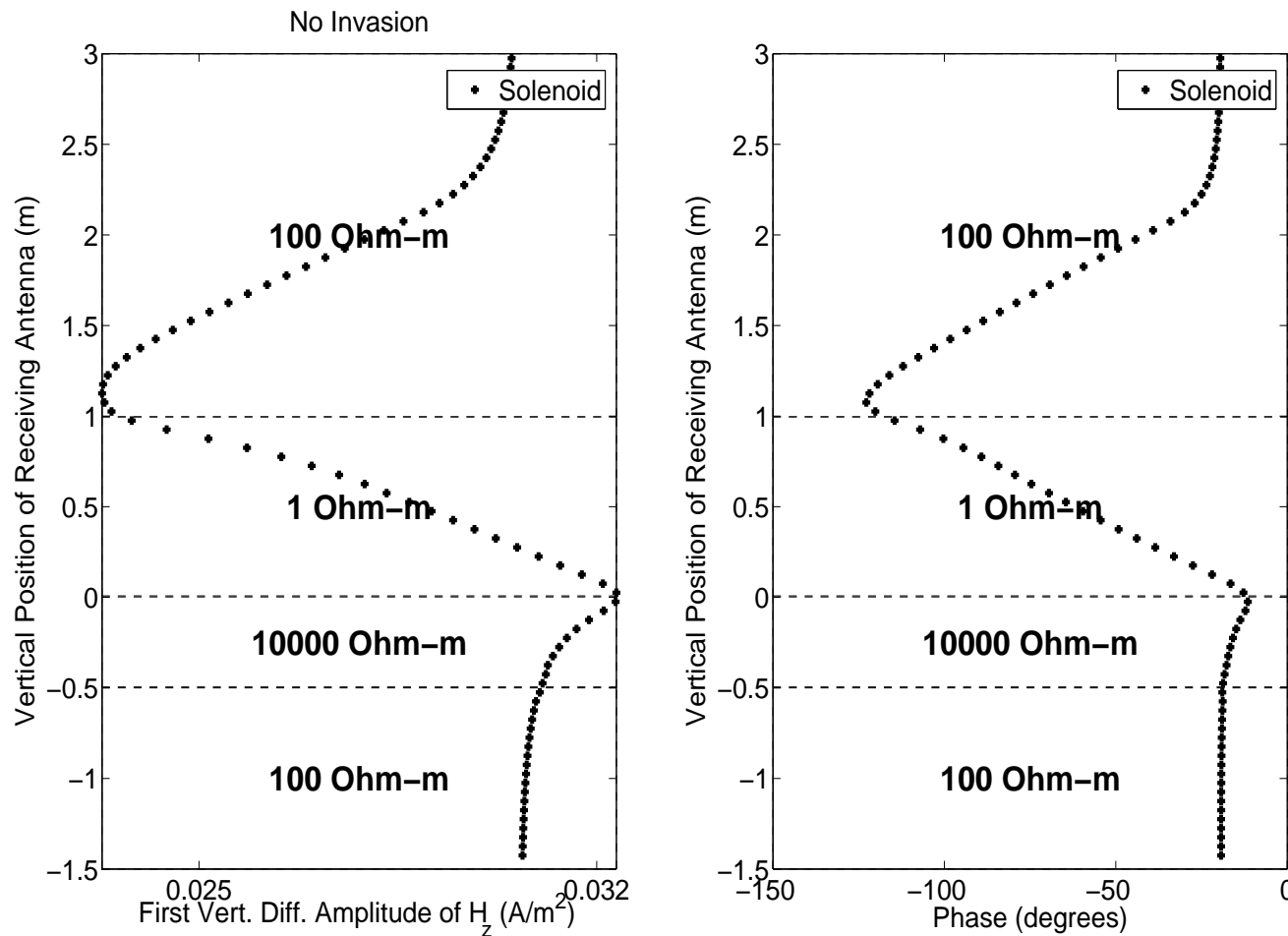
# SIMULATION OF LOGGING INSTRUMENTS

## First Vert. Diff. $E_z$ for a toroid antenna



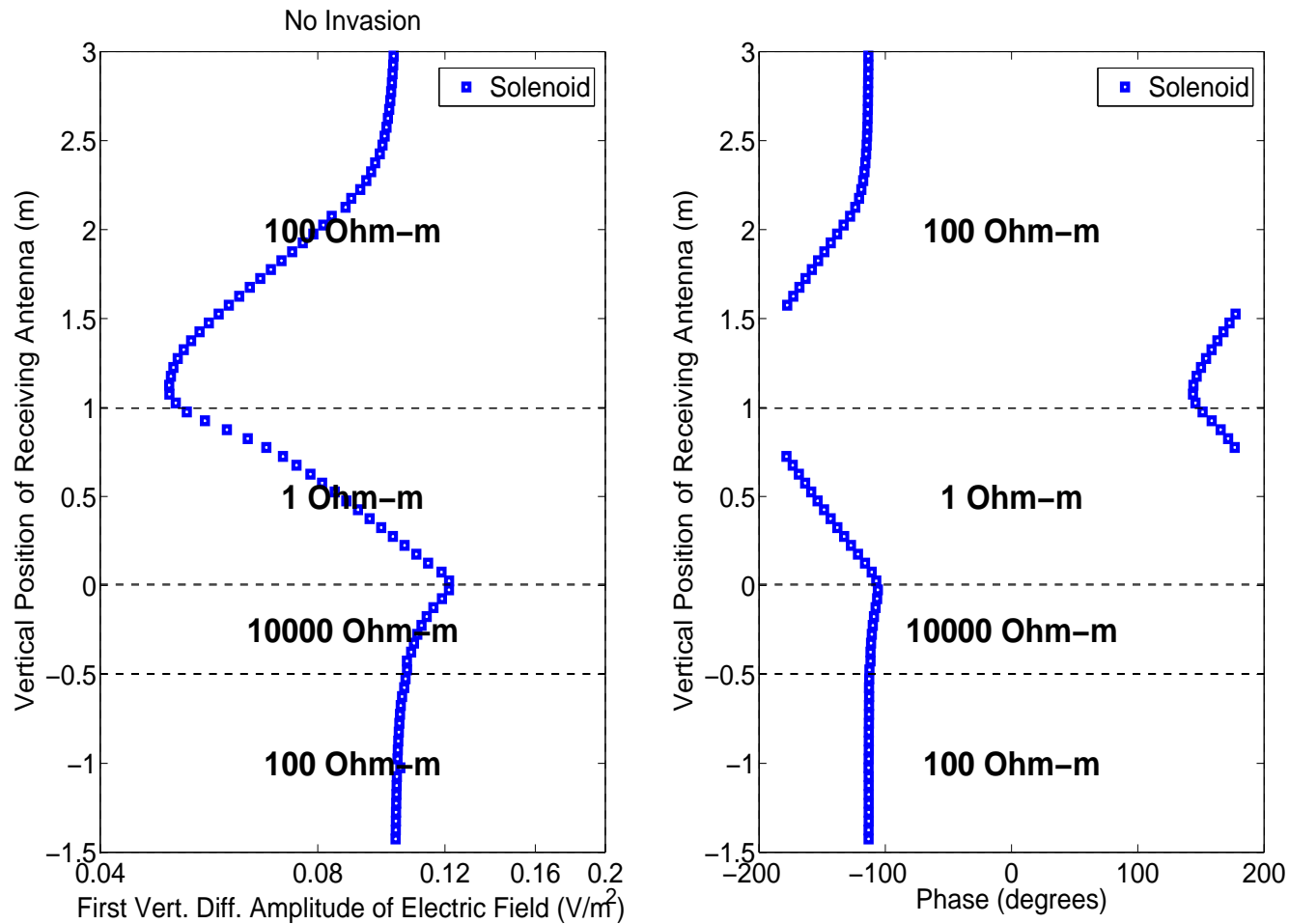
# SIMULATION OF LOGGING INSTRUMENTS

## First Vert. Diff. $H_z$ for a solenoid antenna



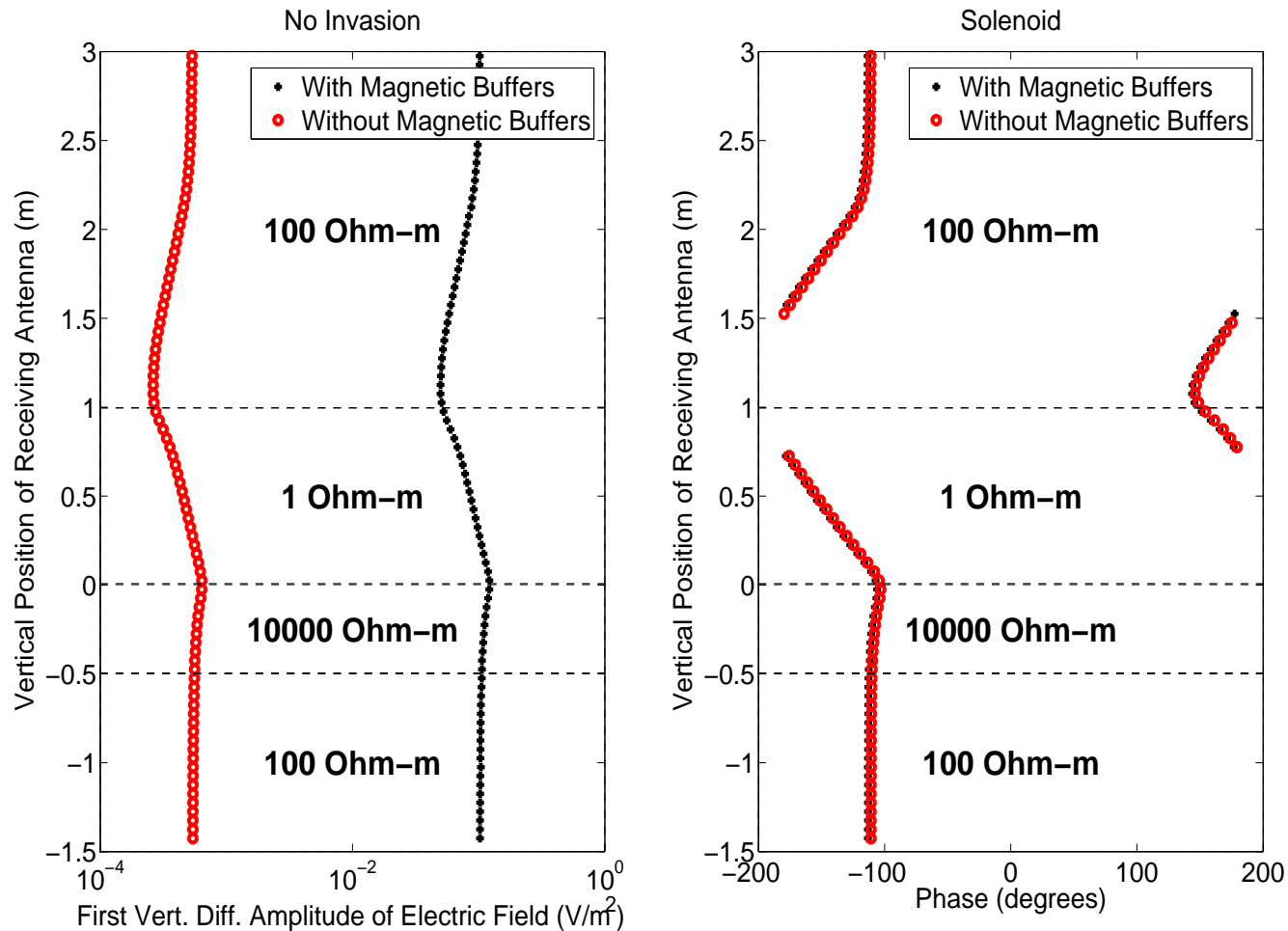
# SIMULATION OF LOGGING INSTRUMENTS

## First Vert. Diff. $E_\phi$ for a solenoid antenna



# SIMULATION OF LOGGING INSTRUMENTS

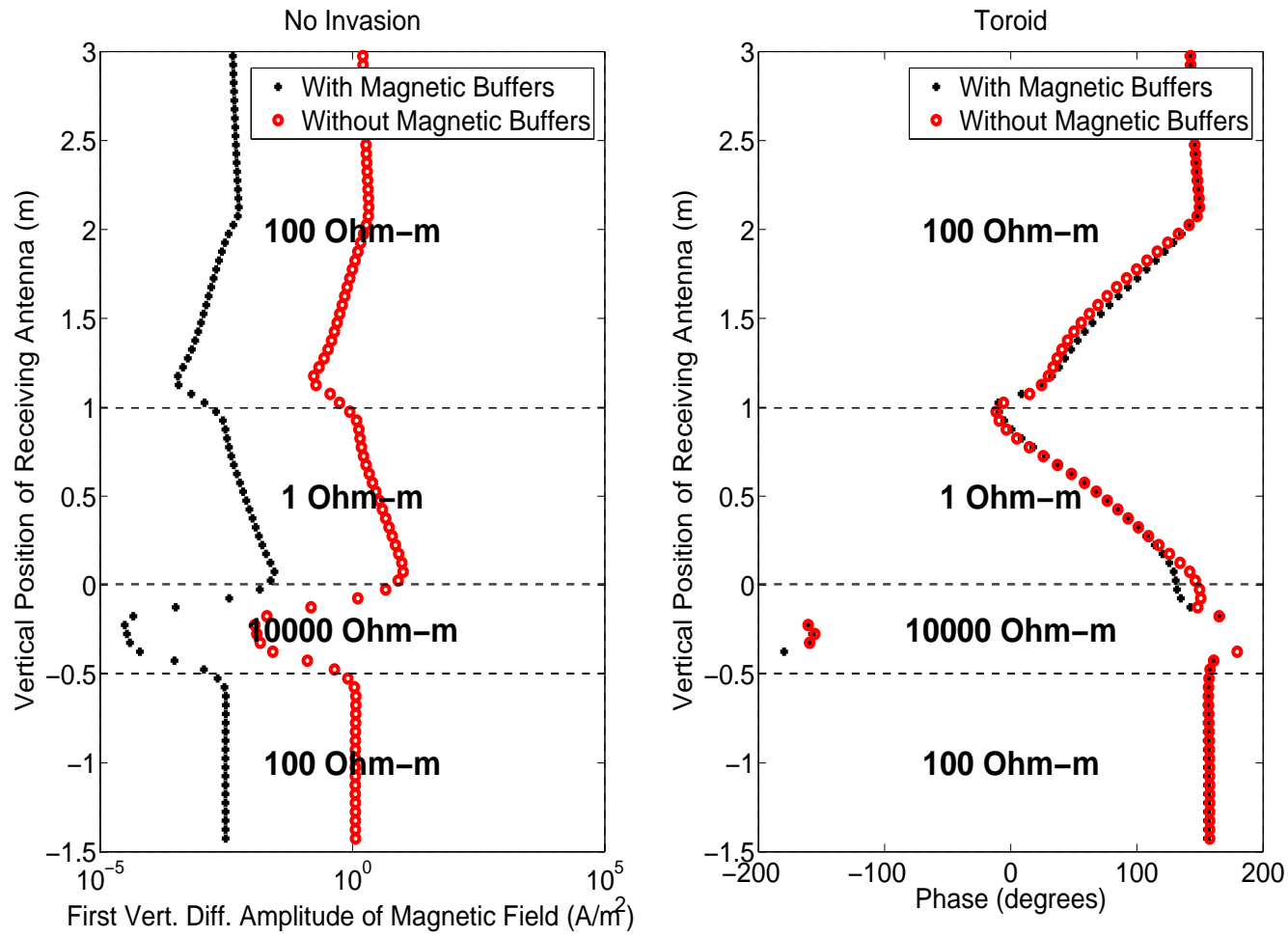
## Use of Magnetic Buffers ( $E_\phi$ for a solenoid)





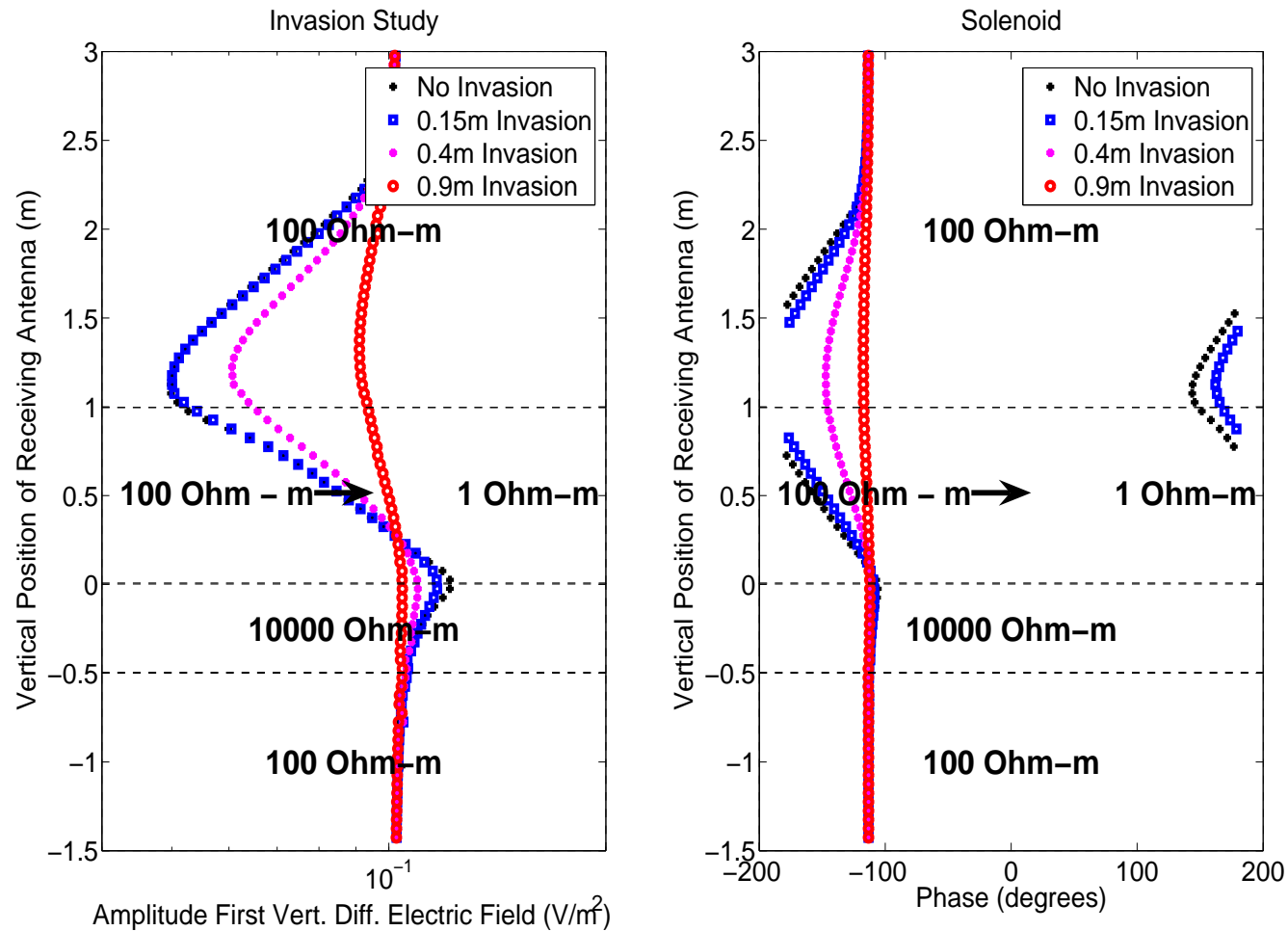
# SIMULATION OF LOGGING INSTRUMENTS

## Use of Magnetic Buffers ( $H_\phi$ for a toroid)



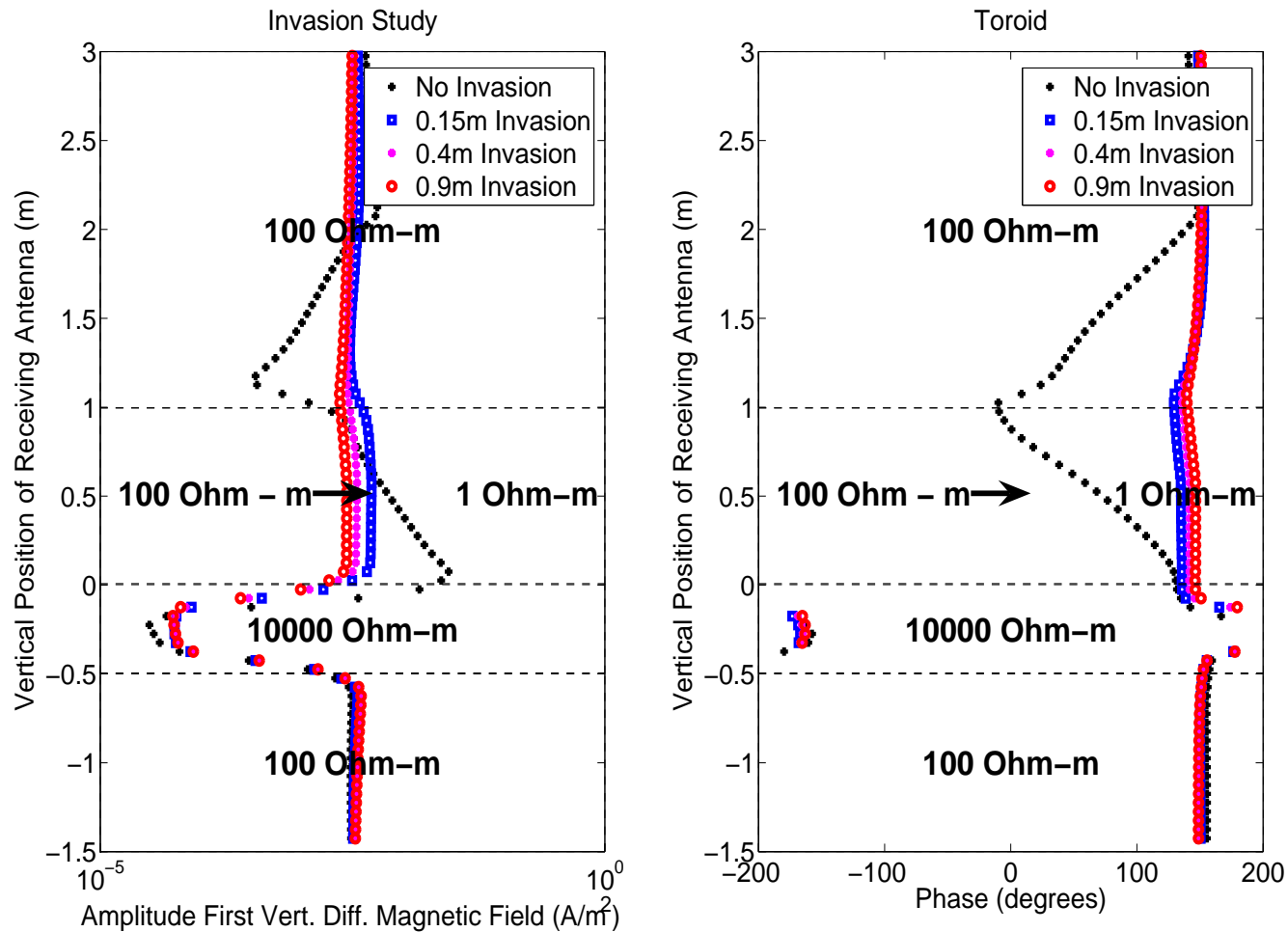
# SIMULATION OF LOGGING INSTRUMENTS

## Invasion study ( $E_\phi$ for a solenoid)



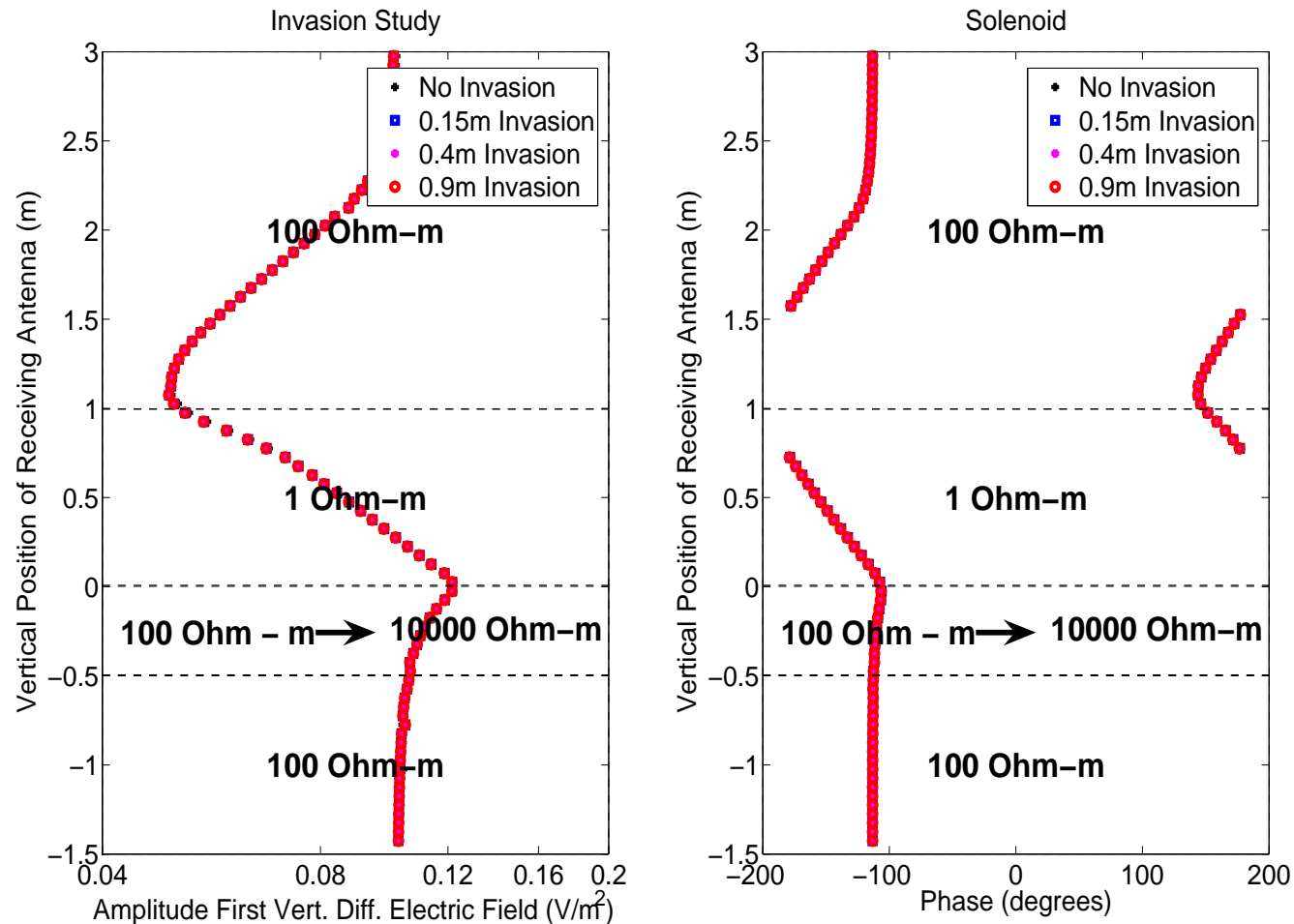
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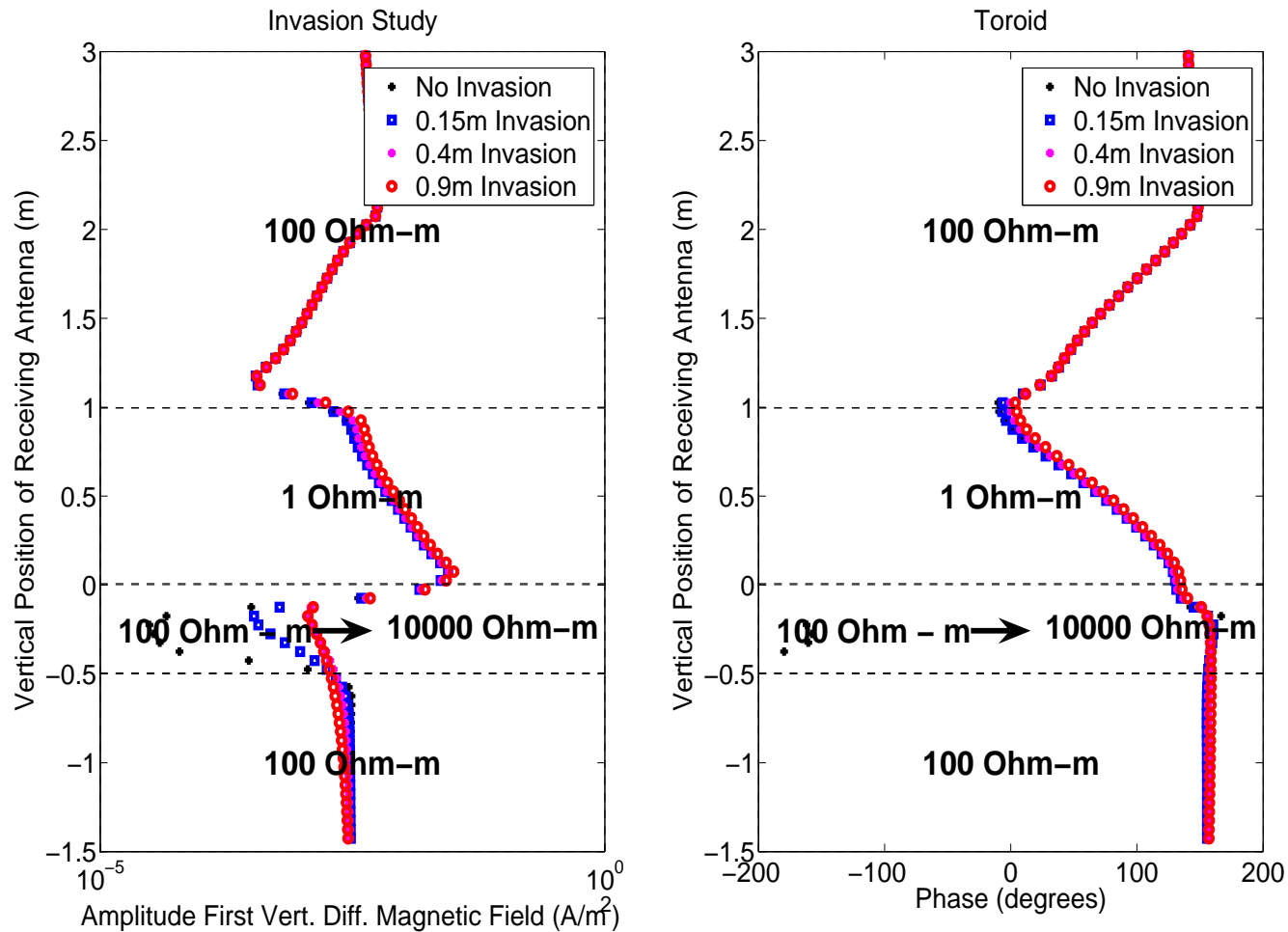
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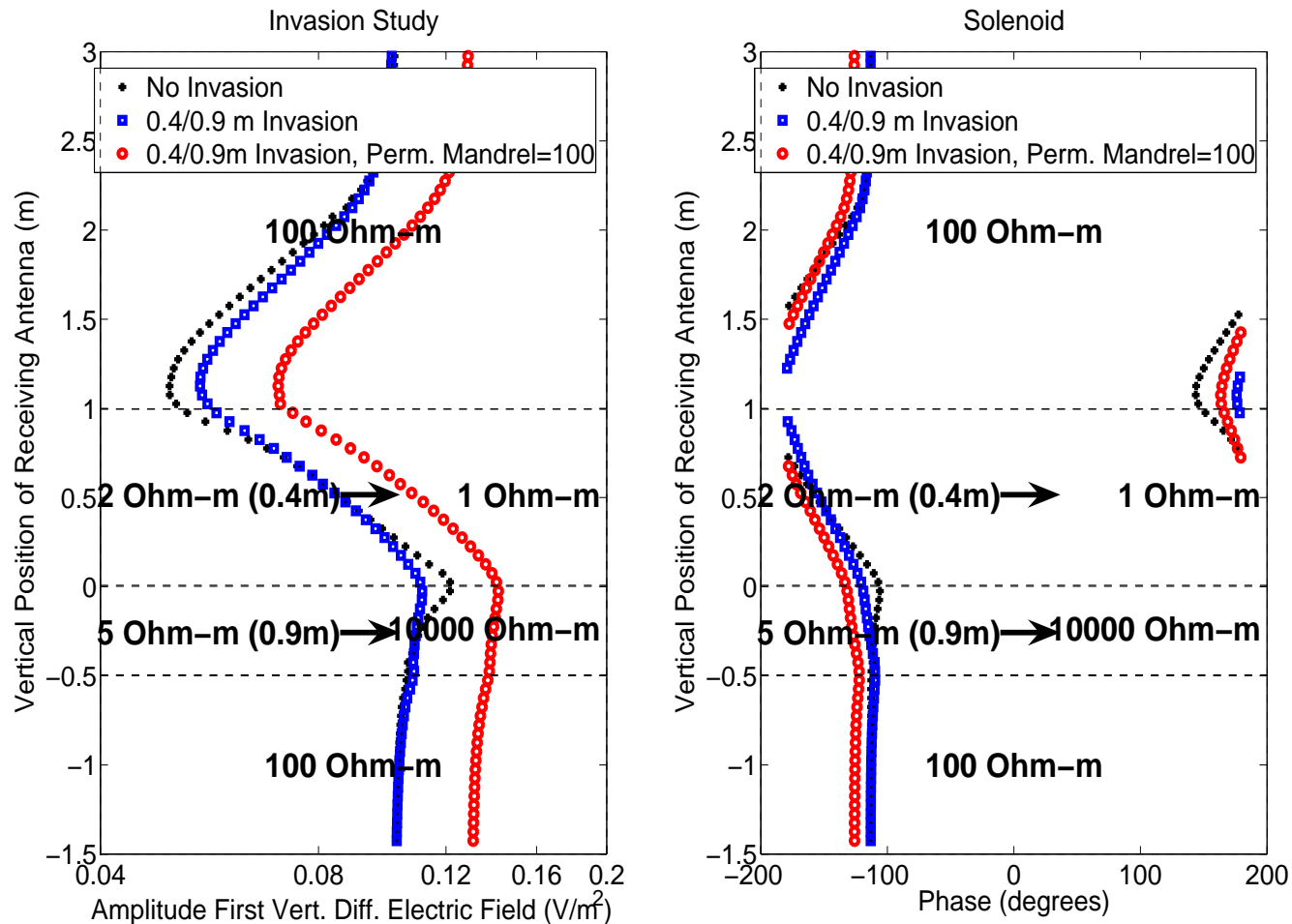
# SIMULATION OF LOGGING INSTRUMENTS

## Invasion study ( $H_\phi$ for a toroid)



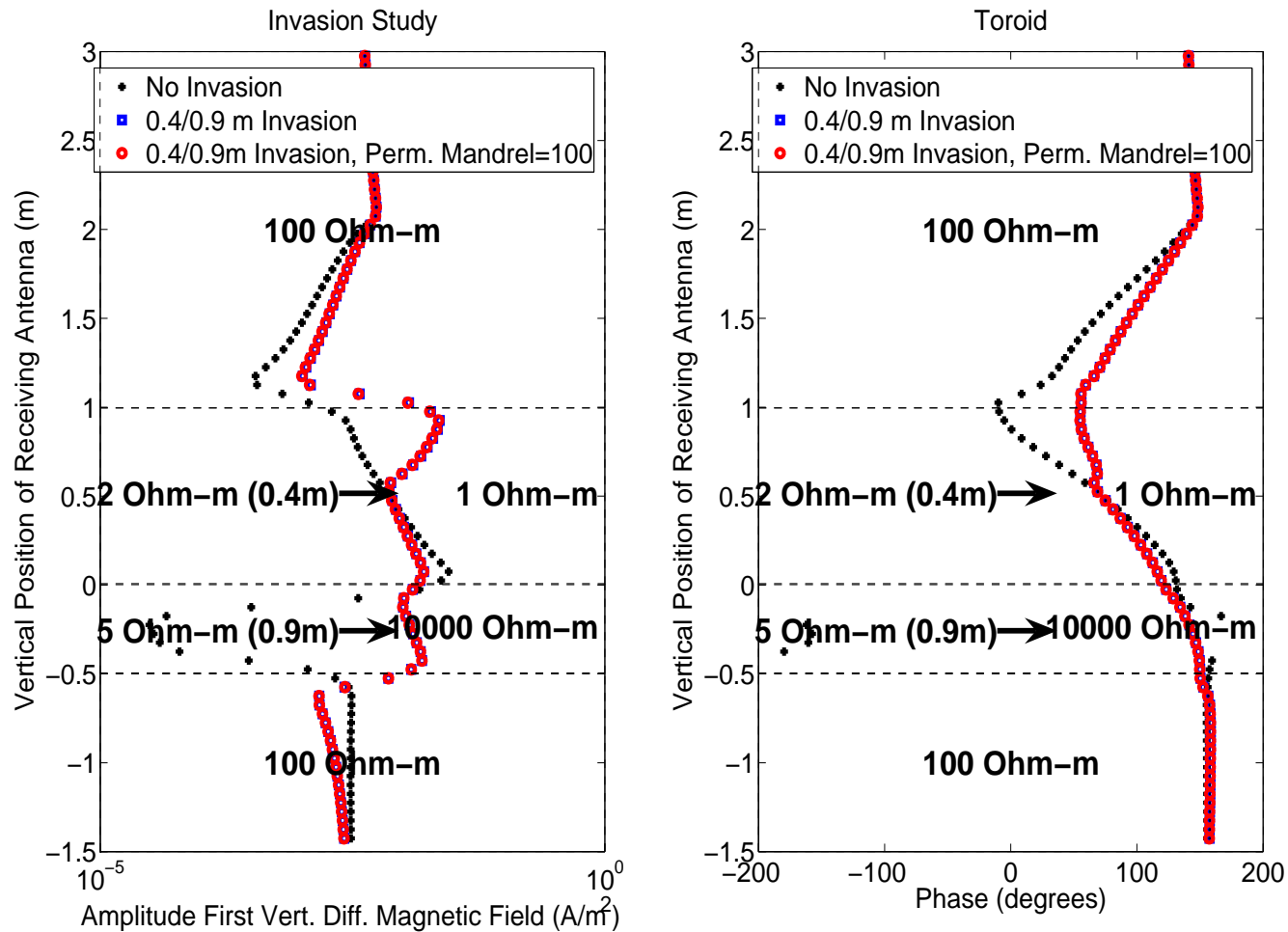
# SIMULATION OF LOGGING INSTRUMENTS

## Invasion and mandrel magnetic permeab. ( $E_\phi$ )



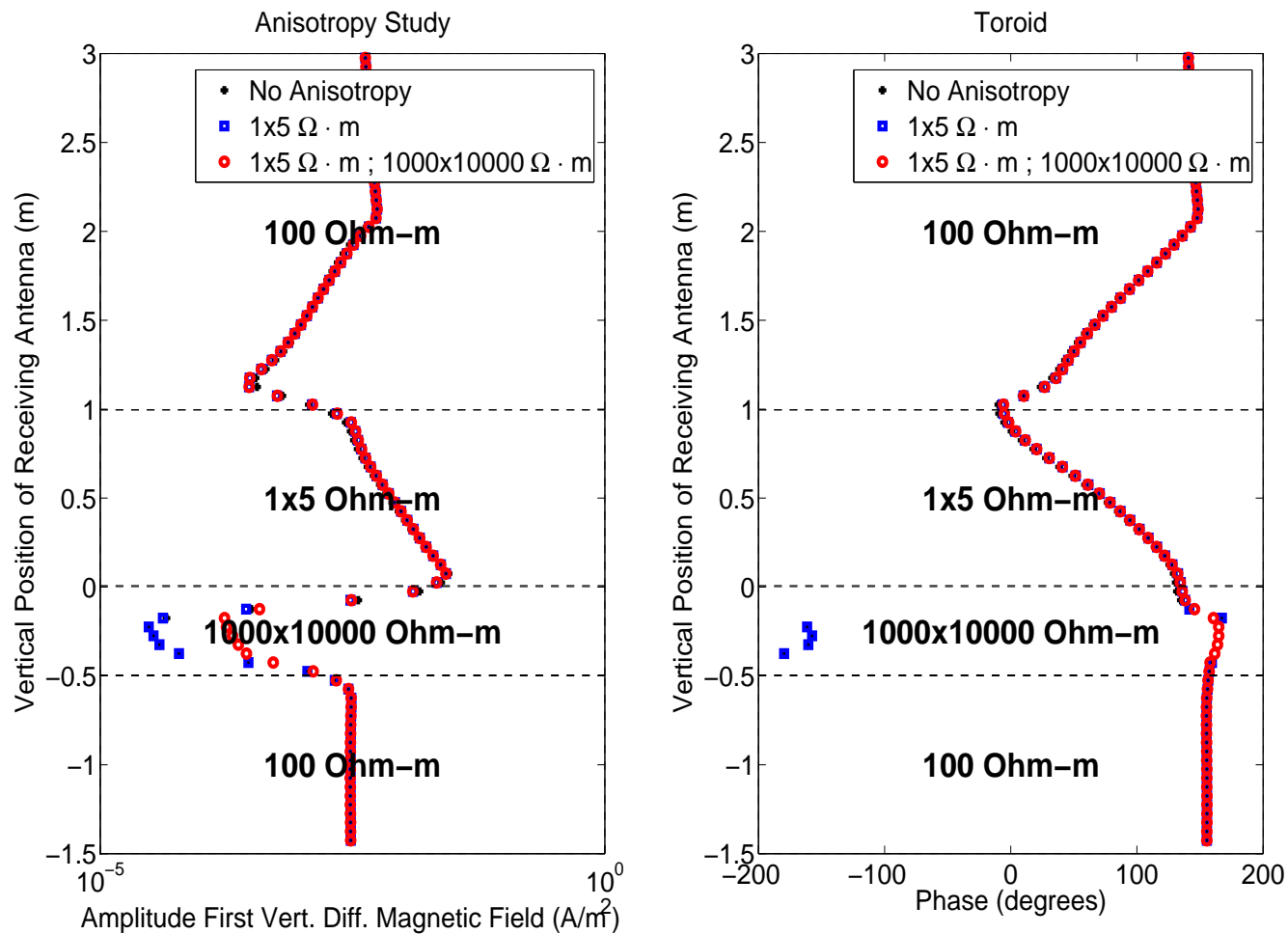
# SIMULATION OF LOGGING INSTRUMENTS

## Invasion and mandrel magnetic permeab. ( $H_\phi$ )



# SIMULATION OF LOGGING INSTRUMENTS

## Anisotropy ( $H_\phi$ )





## CONCLUSIONS AND FUTURE WORK

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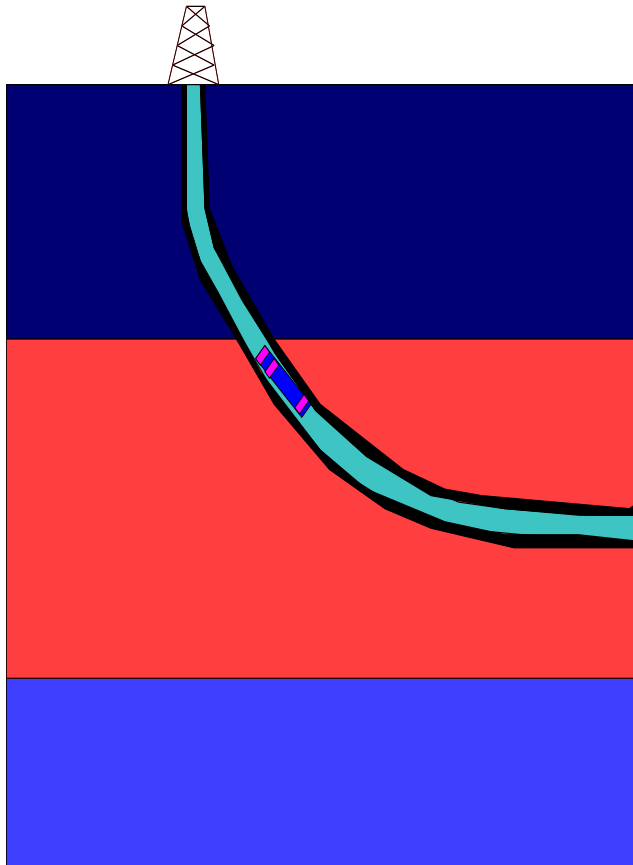
- It is possible to simulate ANY axisymmetric resistivity logging instruments with mandrel (for example, LWD) by using the self-adaptive goal-oriented *hp*-FEM.
- We obtaine fast, reliable and accurate solutions.
- For the discussed LWD problem, numerical results suggest to:
  1. Measure first vertical differences of the EM fields.
  2. Use solenoids for formations with low resitivity, and toroids for highly resistive formations.
  3. Use magnetic buffers in combination with solenoids, not with toroids.
  4. Use solenoids for studying invasion in formations with low resitivity. Use toroids for studying invasion in highly resistive formations.

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# FUTURE WORK

## Simulation of 3D Resistivity Logging Problems



- **PART I: Simulate 3D DC Resistivity Logging Problems.**
  - Estimated completion time: 8-10 months (40 hours/week).
  - Main challenge: Speed.
  - Expected results: Similar results as in 2D.
- **PART II: Simulate 3D AC Resistivity Logging Problems.**
  - Estimated completion time: 8-10 months (40 hours/week).
  - Main challenge: Speed and Implementation.
  - Expected results: Similar results as in 2D.